

PATENT APPLICATION

**ELECTROSURGICAL APPARATUS AND METHODS FOR
CUTTING TISSUE**

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5 CROSS-REFERENCES TO RELATED APPLICATIONS

Sub A 1 → The present invention claims priority from U.S. Provisional Patent Application No. 60/326,664 filed October 2, 2001 (Attorney Docket No. G-4P), and is a continuation-in-part of U.S. Patent Application No. 09/780,745, filed 10 February 9, 2001, (Attorney Docket No. G-2), which claims priority from U.S. Provisional Patent Application No. 60/182,751, filed February 16, 2000, and is a continuation-in-part of U.S. Patent Application No. 09/162,117, filed September 28, 1998, now U.S. Patent No. 6,117,109 (Attorney Docket D-8), which is a continuation in part of U.S. Patent Application No. 08/977,845, filed November 25, 15 1997, now U.S. Patent No. 6,210,402 (Attorney Docket D-2), which is a continuation-in-part of Application No. 08/562,332, filed November 22, 1995, now U.S. Patent No. 6,024,733 (Attorney Docket 016238-000710), and U.S. Patent Application No. 09/041,934, filed March 13, 1998 (Attorney Docket A-1-6), which is a continuation-in-part of U.S. Patent Application No. 08/485,219 filed on June 7, 20 1995, now U.S. Patent No. 5,697,281, (Attorney Docket 16238-000600) the complete disclosures of which are incorporated herein by reference for all purposes. The present invention also claims priority from commonly assigned U.S. Provisional Application No. 60/299,094 filed June 18, 2001 (Attorney Docket No. CB-11P), the complete disclosure of which is incorporated herein by reference for 25 all purposes.

The present invention is also related to commonly assigned co-pending U.S. Provisional Patent Application No. 60/062,996, filed October 23, 1997 (Attorney Docket 16238-007300), U.S. Patent Application No. 08/990,374, filed December 15, 1997, now U.S. Patent No. 6,109,268 (Attorney Docket E-3), 30 which is a continuation-in-part of U.S. Patent Application No. 08/485,219, filed on June 7, 1995, now U.S. Patent No. 5,697,281 (Attorney Docket 16238-000600), Patent Application Nos. 09/109,219, filed on June 30, 1998, 09/058,571, filed on April 10, 1998, now U.S. Patent No. 6,142,992, 08/874,173 filed on June 13, 1997, now U.S. Patent No. 6,179,824 and 09/002,315 filed on January 2, 1998,

now U.S. Patent No. 6,183,469 (Attorney Docket Nos. CB-1, CB-2, 16238-005600 and C-9, respectively) and U.S. Patent Application No. 09/054,323, filed on April 2, 1998, now U.S. Patent No. 6,063,079 (Attorney Docket E-5), U.S. Patent Application No. 09/010,382, filed January 21, 1998, now U.S. patent No.

5 6,190,381 (Attorney Docket A-6), and U.S. Patent Application No. 09/032,375, filed February 27, 1998 (Attorney Docket CB-3), U.S. Patent Application Nos. 08/977,845, filed on November 25, 1997, U.S. Patent No. 6,210,402 (Attorney Docket No. D-2), 08/942,580, filed on October 2, 1997, now U.S. Patent No. 6,159,194 (Attorney Docket 16238-001300), U.S. Patent Application No.

10 08/753,227, filed on November 22, 1996, now U.S. Patent No. 5,873,855 (Docket 16238-002200), U.S. Patent Application No. 08/687,792, filed on July 18, 1996, now U.S. Patent No. 5,843,019 (Docket No. 16238-001600), and PCT International Application, U.S. National Phase Serial No. PCT/US94/05168, filed on May 10, 1994, now U.S. Patent No. 5,697,909 (Attorney Docket 16238-000440), which was

15 a continuation-in-part of U.S. Patent Application No. 08/059,681, filed on May 10, 1993, now abandoned (Attorney Docket 16238-000420), which was a continuation-in-part of U.S. Patent Application No. 07/958,977, filed on October 9, 1992, now U.S. Patent No. 5,366,443 (Attorney Docket 16238-000410) which was a continuation-in-part of U.S. Patent Application No. 07/817,575, filed on January

20 7, 1992 (Attorney Docket 16238-00040), the complete disclosures of which are incorporated herein by reference for all purposes. The present invention is also related to commonly assigned U.S. Patent No. 5,683,366, filed November 22, 1995 (Attorney Docket 16238-000700), the complete disclosure of which is incorporated herein by reference for all purposes.

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BACKGROUND OF THE INVENTION

The present invention generally relates to electrosurgical systems and methods for ablating, severing, dissecting, contracting, or otherwise modifying target tissues or organs. The present invention also relates to electrosurgical

30 apparatus and methods for clamping, compressing, coagulating, welding, occluding, and severing blood vessels during surgical procedures. The invention relates more particularly to electrosurgical apparatus and methods for modifying a tissue or

organ, wherein the apparatus includes an active electrode, a first return electrode fixed with respect to the active electrode, and a second return electrode movable with respect to the active electrode. The present invention still further relates to a laparoscopic electrosurgical probe adapted for cutting, coagulation, and blunt
5 dissection of tissue during laparoscopic procedures.

Conventional electrosurgical instruments and techniques are widely used in surgical procedures because they generally reduce patient bleeding and trauma associated with cutting operations, as compared with mechanical cutting and the like. Conventional electrosurgical procedures may be classified as operating in
10 monopolar or bipolar mode. Monopolar techniques rely on external grounding of the patient, where the surgical device defines only a single electrode pole. Bipolar devices have two electrodes for the application of current between their surfaces. Conventional electrosurgical devices and procedures, however, suffer from a number of disadvantages. For example, conventional electrosurgical cutting devices
15 typically operate by creating a voltage difference between the active electrode and the target tissue, causing an electrical arc to form across the physical gap between the electrode and the tissue. At the point of contact of the electric arcs with the tissue, rapid tissue heating occurs due to high current density between the electrode and the tissue. This high current density causes cellular fluids to rapidly vaporize
20 into steam, thereby producing a "cutting effect" along the pathway of localized tissue heating. Thus, the tissue is parted along the pathway of evaporated cellular fluid, inducing undesirable collateral tissue damage in regions surrounding the target tissue.

Further, monopolar electrosurgical devices generally direct electric
25 current along a defined path from the exposed or active electrode through the patient's body to the return electrode, the latter externally attached to a suitable location on the patient. This creates the potential danger that the electric current will flow through undefined paths in the patient's body, thereby increasing the risk of unwanted electrical stimulation to portions of the patient's body. In addition,
30 since the defined path through the patient's body has a relatively high electrical impedance, large voltage differences must typically be applied between the return and active electrodes in order to generate a current suitable for ablation or cutting of

the target tissue. This current, however, may inadvertently flow along body paths having less impedance than the defined electrical path, which will substantially increase the current flowing through these paths, possibly causing damage to or destroying surrounding tissue.

5 Bipolar electrosurgical devices have an inherent advantage over monopolar devices because the return current path does not flow through the patient. In bipolar electrosurgical devices, both the active and return electrode are typically exposed so that both electrodes may contact tissue, thereby providing a return current path from the active to the return electrode through the tissue. One
10 drawback with this configuration, however, is that the return electrode may cause tissue desiccation or destruction at its contact point with the patient's tissue. In addition, the active and return electrodes are typically positioned close together to ensure that the return current flows directly from the active to the return electrode. The close proximity of these electrodes generates the danger that the current will
15 short across the electrodes, possibly impairing the electrical control system and/or damaging or destroying surrounding tissue.

 In addition, conventional electrosurgical methods are generally ineffective for ablating certain types of tissue, and in certain types of environments within the body. For example, loose or elastic connective tissue, such as the
20 synovial tissue in joints, is extremely difficult (if not impossible) to remove with conventional electrosurgical instruments because the flexible tissue tends to move away from the instrument when it is brought against this tissue. Since conventional techniques rely mainly on conducting current through the tissue, they are not effective when the instrument cannot be brought adjacent to, or in contact with, the
25 elastic tissue for a sufficient period of time to energize the electrode and conduct current through the tissue.

 A number of disadvantages inherent in conventional electrosurgical devices have been set forth hereinabove. There is a need for an electrosurgical apparatus which can be used for the precise removal or modification of tissue at a
30 specific location, wherein a target tissue or organ can be dissected, transected, resected, incised, severed, compressed, contracted, coagulated, occluded, or otherwise modified in a controlled manner.

SUMMARY OF THE INVENTION

The present invention generally provides systems, apparatus, and methods for selectively applying electrical energy to cut, incise, ablate, or otherwise modify a tissue or organ of a patient. In one aspect, apparatus and methods of the invention are useful for electrosurgically cutting and resecting tissue, and for dissecting, coagulating, occluding, and severing veins, arteries or other hollow organs of a patient during a broad range of surgical procedures. For example, in one aspect the present invention provides a laparoscopic probe having a hook-like active electrode adapted for cutting, blunt dissection, and coagulation of tissue. In another aspect of the invention, the probe includes a movable return electrode which is adapted for clamping tissue or a blood vessel against the hook-like active electrode to provide additional coagulation capability.

In one aspect, the present invention provides a method of creating an incision in a body structure. An electrosurgical probe is positioned adjacent the target tissue so that one or more active electrode(s) are brought into at least partial contact or close proximity with the target tissue. High frequency voltage is then applied between the active electrode(s) and one or more return electrode(s) and the active electrode(s) are moved, translated, reciprocated, or otherwise manipulated to cut through a portion of the tissue. In some embodiments, an electrically conductive fluid, e.g., isotonic saline or conductive gel, is delivered or applied to the target site to substantially surround the active electrode(s) with the fluid. In other embodiments, the active electrode(s) are immersed within the electrically conductive fluid. In both embodiments, the high frequency voltage may be selected to locally ablate or sever a target tissue, and/or to effect a controlled depth of hemostasis of severed blood vessels within the tissue. In another aspect, the electrosurgical systems and methods of the invention are useful for harvesting and dissecting veins and arteries of a patient, such as the saphenous vein or the IMA (Internal Mammary Artery) for use in a CABG (Cardiac Arterial By-pass Graft) procedure.

In one aspect, tissue is cut or otherwise modified by molecular dissociation or disintegration processes. (In contrast, in conventional electrosurgery tissue is cut by rapidly heating the tissue until cellular fluids explode, producing a

cutting effect along the pathway of localized heating.) The present invention volumetrically removes the tissue along the cutting pathway in a cool ablation process that minimizes thermal damage to surrounding tissues. In these embodiments, the high frequency voltage applied to the active electrode(s) is
5 sufficient to vaporize the electrically conductive fluid (e.g., gel or saline) between the active electrode(s) and the tissue. Within the vaporized fluid, a plasma is formed and charged particles (e.g., electrons and ions) cause the molecular breakdown or disintegration of the tissue, perhaps to a depth of several cell layers. This molecular dissociation is accompanied by the volumetric removal of the tissue,
10 e.g., along the incision of the tissue. This process can be precisely controlled to effect the volumetric removal of tissue as thin as 10 microns to 150 microns with minimal heating of, or damage to, surrounding or underlying tissue structures. A more complete description of this phenomenon is described in commonly assigned U.S. Patent No. 5,683,366, the complete disclosure of which is incorporated herein
15 by reference.

In a specific embodiment, the present invention provides a method of accessing a patient's thoracic cavity. The active electrode(s) are positioned in contact with, or in close proximity to, a surface of the sternum. A high frequency voltage is applied between the active electrode(s) and a return electrode. The active
20 electrodes are moved across the sternum to create an incision. In a specific configuration, the sides of the active electrode are slidingly engaged with the sternum as the incision is being made, so as to cause coagulation and hemostasis within the sternum.

In another exemplary embodiment, the present invention provides a
25 method for harvesting the IMA from a patient. The electrosurgical probe is positioned adjacent the IMA and high frequency electrical energy is applied between one or more active electrode(s) and one or more return electrode(s). The probe is then moved so that the active electrode(s) volumetrically removes connective tissue adjacent to the IMA so that the IMA is free from connective tissue along a portion
30 of its length. In an exemplary embodiment, the probe is positioned adjacent to the IMA, and advanced along the length of the IMA while high frequency electrical energy is applied between the active electrode(s) and a return electrode to remove or

cut the connective tissue or other structures surrounding the IMA. The residual heat from the electrical energy also provides simultaneous hemostasis of severed blood vessels, which increases visualization and improves recovery time for the patient.

In addition, the ability to simultaneously cut through tissue on either side of the

5 IMA decreases the length of the procedure, which further improves patient recovery time. After a suitable length of the IMA has been dissected, it may be transected, and anastomosed to a diseased coronary artery using known methods. In some embodiments, an electrically conductive fluid (liquid, gas, or gel) is placed at the target site adjacent to the IMA so as to provide a current flow path between the
10 return electrode and the active electrode.

Apparatus according to the present invention generally include an electrosurgical instrument, such as a probe or catheter, having a shaft with proximal and distal ends, one or more active electrode(s) at the distal end and one or more connectors coupling the active electrode(s) to a source of high frequency electrical
15 energy. The active electrode(s) are preferably designed for cutting tissue, i.e., they typically have a distal edge or point. In one embodiment, a plurality of active electrodes are aligned with each other to form a linear electrode array for cutting a path through the tissue. In another exemplary embodiment, the active electrode(s) include a sharp distal point to facilitate the cutting of the target tissue. In one
20 specific configuration, the active electrode is a blade having a sharp distal point and sides. As the sharp distal point incises the tissue, the sides of the blade slidably contact the incised tissue. The electrical current flows through that portion of the tissue in the vicinity of the active electrode and/or the conductive fluid to the return electrode, such that the target tissue is first severed, and then the severed tissue is
25 coagulated.

The apparatus can further include a fluid delivery element for delivering electrically conductive fluid to the active electrode(s) and the target site. The fluid delivery element may be located on the probe, e.g., a fluid lumen or tube, or it may be part of a separate instrument. Alternatively, an electrically conductive
30 gel or spray, such as a saline electrolyte or other conductive gel, may be applied the target site. In this embodiment, the apparatus may not have a fluid delivery element. In both embodiments, the electrically conductive fluid preferably provides

a current flow path between the active electrode(s) and one or more return electrode(s). In an exemplary embodiment, the return electrode is located on the probe and spaced a sufficient distance from the active electrode(s) to substantially avoid or minimize current shorting therebetween and to shield the return electrode from tissue at the target site.

In a specific configuration, the electrosurgical probe includes an electrically insulating electrode support member having a tissue treatment surface at the distal end of the probe. One or more active electrode(s) are coupled to, or integral with, the electrode support member such that the active electrode(s) are spaced from the return electrode. In one embodiment, the probe includes a plurality of active electrode(s) having distal edges linearly aligned with each other to form a sharp cutting path for cutting tissue. The active electrodes are preferably electrically isolated from each other, and they extend about 0.2 mm to about 10 mm distally from the tissue treatment surface of the electrode support member. In this embodiment, the probe may further include one or more lumina (or lumens) for delivering electrically conductive fluid to one or more openings around the tissue treatment surface of the electrode support member. In one embodiment, the lumen extends through a fluid tube exterior to the probe shaft that ends proximal to the return electrode.

In another aspect of the invention, there is provided an electrosurgical probe including a shaft and a fixed electrode assembly disposed at the shaft distal end. The fixed electrode assembly includes an active electrode and a first return electrode fixed in relation to the active electrode. The probe further includes a second return electrode movable in relation to the active electrode, wherein the second return electrode is movable between a proximal location defining an open configuration of the probe, and a distal location defining a closed configuration of the probe. Typically, the movable, second return electrode is movable linearly with respect to the shaft between the proximal location and the distal location in a direction parallel to the longitudinal axis of the shaft. In one embodiment, the active electrode comprises a hook-like active electrode terminal. In use, the active electrode and the return electrode are coupled to opposite poles of a high frequency power supply. The active electrode terminal and the moveable return electrode are

adapted for clamping tissue or a blood vessel, and for coagulating or welding the tissue or blood vessel in the sub-ablation mode. The active electrode terminal is further adapted for cutting, resecting, or severing tissue, or a blood vessel, in the ablation mode.

5 In another aspect of the invention, there is provided an electrosurgical probe including a shaft and an electrically insulating tube lying within the shaft, wherein the tube extends distally from the shaft distal end to define a first electrically insulating spacer. The probe further includes a fixed, first return electrode disposed at the distal end of the first spacer, and a second electrically
10 insulating spacer extending distally from the fixed return electrode. An active electrode terminal is disposed at the distal end of the second spacer. The probe further includes a second return electrode movable in relation to the active electrode terminal, wherein the movable return electrode is movable linearly between a proximal location and a distal location in a direction parallel to the longitudinal axis
15 of the shaft. The proximal location of the movable return electrode defines an open configuration of the probe, and the distal location of the movable return electrode defines a closed configuration of the probe. In one embodiment, the movable return electrode slides internal to the shaft and external to the electrically insulating tube. According to one aspect of the invention, the electrically insulating tube comprises a
20 multi-lumen plastic tube formed by an extrusion process. Such a multi-lumen plastic tube may accommodate an aspiration lumen for proximal passage of an aspiration stream, a fluid delivery lumen for delivery of electrically conductive fluid to the working end of the probe, as well as lumina for active and return electrode filaments or leads.

25 An electrosurgical probe of the invention may be provided in various configurations, for example, according to a particular procedure to be performed. Thus, the active electrode terminal may be provided in various forms, such as a shaped, flattened, and/or bent wire, or a metal blade, e.g., a metal disc, or portion thereof, or a hook comprising a crosspiece supported by at least one electrode arm,
30 The crosspiece may be arranged at various angles to the arm, e.g., an angle of about 45° to the arm, or the crosspiece may be substantially orthogonal to the arm. In one embodiment, the active electrode terminal comprises a shaped wire having a

plurality of contiguous planar surfaces. In a specific configuration according to one embodiment of the invention, the active electrode includes an axial electrode arm or filament comprising a pair of juxtaposed wires, and a crosspiece comprising a first branch and a second branch tapering in a direction away from the electrode arm to a bent apical portion of the crosspiece. An elongated window or void located between the first branch and the second branch is adapted for retaining and transporting a liquid within the window via capillary action (or capillary attraction). The distal end of the movable return electrode may be straight or beveled, and may be circular or semi-circular in cross-section. Each of these features or elements of the probe may facilitate accessing, engaging, and/or grasping a tissue or organ targeted for treatment or modification by the probe.

According to another aspect, the invention provides a laparoscopic probe having a hook-like active electrode and a movable return electrode, wherein the probe is adapted for ablating tissue (e.g., via Coblation®). The probe is further adapted for clamping soft tissue or a blood vessel between the movable return electrode and the active electrode, and for coagulating the tissue or blood vessel thus clamped. The probe may be used in a broad range of laparoscopic procedures, including without limitation: myomectomy, cystectomy, lysis of adhesions, and laparoscopic cholecystectomy (lap choles).

In another aspect of the invention, there is provided a method for ablating, cutting, severing, coagulating, welding, contracting, or otherwise modifying a tissue or organ using an electrosurgical probe having an active electrode, a first return electrode fixed in relation to the active electrode, and a second return electrode movable in relation to the active electrode. The second return electrode is movable between a proximal location defining an open configuration of the probe, and a distal location defining a closed configuration of the probe. The method involves applying a high frequency voltage between the active electrode and at least one of the first return electrode and the second return electrode.

In one embodiment, a method of the invention involves clamping a blood vessel between an active electrode terminal and a movable return electrode, whereby the blood vessel is compressed to substantially prevent blood flow through

the vessel. While the blood vessel is thus compressed, the method further involves applying a first high frequency voltage between the active electrode and the movable return electrode in the sub-ablation mode, whereby the walls of the blood vessel are welded together and the vessel is occluded. Thereafter, a second high frequency voltage may be applied between the active electrode and a fixed return electrode in the ablation mode, whereby the blood vessel is severed while maintaining hemostasis.

Apparatus of the invention is applicable to a broad range of procedures, including without limitation: cutting, resection, ablation, and/or hemostasis of tissues and organs such as prostate tissue, scar tissue, myocardial tissue, and tissues of the knee, shoulder, hip, and other joints; procedures of the head and neck, such as of the ear, mouth, throat, pharynx, larynx, esophagus, nasal cavity, and sinuses; as well as procedures involving skin tissue removal and/or collagen shrinkage in the epidermis or dermis. A more detailed account of various treatments and procedures which may be carried out according to the invention is set forth in enabling detail hereinbelow.

For a further understanding of the nature and advantages of the invention, reference should be made to the following description taken in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a perspective view of an electrosurgical system incorporating a power supply and an electrosurgical probe for tissue ablation, resection, incision, contraction, vessel harvesting, and hemostasis, according to the present invention;

Fig. 2 is a side view of an electrosurgical probe according to the present invention;

Fig. 3 is an end view of the distal portion of the probe of Fig. 2;

Fig. 4 is a cross sectional view of the distal portion of the electrosurgical probe of Fig. 2;

Fig. 5 is an exploded view of a proximal portion of the electrosurgical probe;

Fig. 6 is an end view of an exemplary electrode support comprising a multi-layer wafer with plated conductors for electrodes;

Figs. 7 and 8 are side views of the electrode support of Fig. 7;

5 Figs. 9A-13 are side views of the individual wafer layers of the electrode support;

Figs. 9B-12B are cross-sectional views of the individual wafer layers;

Figs. 14 and 15 illustrate an alternative multi-layer wafer design according to the present invention;

10 Fig. 16 is a perspective view of an electrosurgical probe having an elongated, blade-like active electrode;

Figs. 17A-17C are cross-sectional views of the distal portions of three different embodiments of an electrosurgical probe according to the present invention;

15 Fig. 18 illustrates an electrosurgical probe with a 90° distal bend and a lateral fluid lumen;

Fig. 19 illustrates an electrosurgical system with a separate fluid delivery instrument according to the present invention;

Figs. 20A and 20B are cross-sectional and end views, respectively, of yet another electrosurgical probe incorporating flattened active electrodes;

20 Fig. 21 is a detailed end view of an electrosurgical probe having an elongate, linear array of active electrodes suitable for use in surgical cutting;

Fig. 22 is a detailed view of a single active electrode having a flattened end at its distal tip;

25 Fig. 23 is a detailed view of a single active electrode having a pointed end at its distal tip;

Fig. 24 is a perspective view of the distal portion of another electrosurgical probe according to the present invention;

Fig. 25 illustrates another embodiment of the probe of the present invention, specifically designed for creating incisions in external skin surfaces;

30 Fig. 26 is a perspective view of another embodiment of an electrosurgical probe for use in dermatology procedures;

Figs. 27A-27C are exploded, isometric views of the probe of Fig. 26;

Fig. 28 is a cross-sectional view of another alternative electrosurgical probe;

Fig. 29 illustrates another embodiment of the electrosurgical probe of the present invention, incorporating additional active electrodes;

5 Fig. 30 is a perspective view of an electrosurgical probe having a blade electrode;

Fig. 31A is a perspective view, and Fig. 31B is a lateral view, of a blade electrode, according to one embodiment of the invention;

10 Figs. 32A, 32B, and 32C are a side view, a plan view, and an end view, respectively, of an electrosurgical probe having a blade electrode;

Figs. 33A and 33B are a side view and a plan view, respectively, of the distal end of an electrosurgical probe having a terminal blade electrode, according to one embodiment of the invention;

15 Figs. 33C-33E each show a side view of the distal end of an electrosurgical probe having a terminal blade electrode, according to three different embodiments of the invention;

Figs. 34A, 34B, and 34C are a side view, a plan view, and an end view, respectively, of an electrosurgical probe having a terminal electrode support and a lateral blade electrode, according to another embodiment of the invention;

20 Figs. 35A, 35B, and 35C are a side view, a plan view, and an end view, respectively, of an electrosurgical probe having a lateral electrode support and a lateral blade electrode, according to another embodiment of the invention;

25 Figs. 36A and 36B each show a side view of the distal end of an electrosurgical probe having a blade electrode, according to two different embodiments of the invention;

Figs. 37A and 37B are a side view and an end view, respectively, of an electrosurgical probe having a lumen external to the probe shaft, according to one embodiment of the invention;

30 Figs. 38A, and 38B are a side view and an end view, respectively, of an electrosurgical probe having an outer sheath surrounding the probe shaft, according to another embodiment of the invention;

Figs. 39A, 39B, and 39C schematically represent a perspective view, a longitudinal sectional view, and an end view, respectively, of an electrosurgical probe, according to another embodiment of the invention;

Fig. 39D shows detail of the distal portion of the probe of Figs. 39A-
5 C;

Figs. 40A and 40B schematically represent a longitudinal sectional view, and an end view, respectively, of an electrosurgical probe, according to another embodiment of the invention;

Fig. 40C shows detail of the distal portion of the probe of Figs. 40A,
10 40B;

Figs. 41A, 41B, and 41C each show detail of the distal portion of an electrosurgical probe, according to three different embodiments of the invention;

Figs. 42A and 42B schematically represent a procedure for incising and coagulating tissue with an electrosurgical probe having a blade electrode,
15 according to one embodiment of the invention;

Fig. 43A schematically represents a number of steps involved in a method of treating a patient with an electrosurgical probe having a blade electrode, according to one embodiment of the invention;

Fig. 43B schematically represents a number of steps involved in a
20 method of concurrently severing and coagulating tissue, according to one embodiment of the invention;

Fig. 44 schematically represents a number of steps involved in a method of dissecting a tissue or organ of a patient with an electrosurgical probe, according to another embodiment of the invention;

Figs. 45A and 45B are block diagrams, each schematically
25 representing an electrosurgical system of the instant invention;

Fig. 46 is a block diagram schematically representing an electrosurgical probe according to the invention;

Figs. 47A and 47B schematically represent an electrosurgical probe
30 having a linearly movable return electrode, according to one embodiment of the invention;

Figs. 48A and 48B schematically represent an electrosurgical probe having a return electrode movable between electrical engagement and electrical disengagement, according to one embodiment of the invention;

5 Figs. 49A and 49B schematically represent an electrosurgical probe having a return electrode movable between electrical engagement and electrical disengagement, according to another embodiment of the invention;

Fig. 50 is a block diagram schematically representing an electrosurgical probe, according to another embodiment of the invention;

10 Figs. 51A and 51B schematically represent an electrosurgical probe, having a linearly movable return electrode in a proximal location and a distal location, respectively;

Fig. 51C is a transverse section taken along the lines 51C-51C of Fig. 51A;

15 Figs. 52A-C each show the distal end of an electrosurgical probe having a linearly movable return electrode, according to one embodiment of the invention;

Figs. 53A-C schematically represent occlusion of a blood vessel by an electrosurgical probe having a linearly movable return electrode, according to one embodiment of the invention;

20 Figs. 54A and 54B are longitudinal and transverse sectional views, respectively, of a movable return electrode/push rod assembly having a circular cross-section and an exposed, beveled distal end;

Fig. 54C is a side view of a movable return electrode adjacent to an active electrode terminal;

25 Figs. 54D and 54E are longitudinal and transverse sectional views, respectively, of a movable return electrode/push rod assembly having a circular cross-section and a straight distal end;

30 Figs. 54F and 54G are longitudinal and transverse sectional views, respectively, of a movable return electrode/push rod assembly having a semi-circular cross-section and an exposed, beveled distal end;

Figs. 55A and 55B schematically represent a hook-like active electrode terminal, according to one embodiment of the invention;

Fig. 55C schematically represents a hook-like active electrode terminal, according to another embodiment of the invention;

Figs. 55D-F schematically represent a hook-like active electrode, according to another embodiment of the invention;

5 Fig. 56A schematically represents a multi-lumen tube for an electrosurgical probe, according to one aspect of the invention;

Fig. 56B schematically represents a multi-lumen tube, in perspective view, according to one embodiment the invention;

10 Fig. 56 C is an end view of the multi-lumen tube of Fig. 56B showing a plurality of ports on an end plate of the tube in relation to a probe shaft;

Fig. 56D shows the location of an active electrode filament and a return electrode in relation to the plurality of ports of the multi-lumen tube of Figs. 56B, 56C;

15 Fig. 57A is a side view of a fixed return electrode in relation to the distal end of a multi-lumen tube, according to one embodiment of the invention;

Fig. 57B is a side view of the distal portion of an electrosurgical probe including an active electrode and the return electrode of Fig. 57A, according to one embodiment of the invention;

20 Fig. 57C is an end view of the return electrode of Fig. 57B showing an electrically insulating spacer encircling an active electrode filament within the return electrode, according to one embodiment of the invention;

Fig. 58A is an end view of the distal face of a multi-lumen tube indicating a location of an electrode assembly in relation to a fluid delivery port and an aspiration port, according to another aspect of the invention;

25 Fig. 58B is a side view of the multi-lumen tube of Fig. 58A;

Fig. 59A is a side view of an electrosurgical probe in the open configuration, with a movable return electrode retracted in a proximal location within the probe shaft, according to one embodiment of the invention;

30 Fig. 59B is a side view of the electrosurgical probe of Fig. 59A in the closed configuration, with the movable return electrode in a distal location adjacent to an active electrode;

Fig. 59C is a sectional view taken along the lines 59C-59C of Fig. 59B;

Fig. 60A schematically represents a number of steps involved in a method of treating a target tissue of a patient with an electrosurgical probe,

5 according to another embodiment of the invention; and

Figs. 60B and 60C each schematically represents a number of steps involved in a method of severing a tissue of a patient, according to another embodiment of the invention.

10 DESCRIPTION OF THE SPECIFIC EMBODIMENTS

The present invention provides systems and methods for selectively applying electrical energy to a target location within or on a patient's body, particularly for cutting, ablating, coagulating, or otherwise modifying a tissue, blood vessel, or organ. The instant invention also provides apparatus and methods
15 for making incisions to access a tissue or organ within a patient's body, to dissect or harvest the tissue or organ from the patient, and to transect or otherwise modify the tissue or organ. In one aspect, the invention provides apparatus and methods for cutting, resecting, and dissecting tissue, and for clamping, coagulating, and severing blood vessels.

20 The present invention is useful in procedures where the target tissue or organ is, or can be, flooded or submerged with an electrically conductive fluid, such as isotonic saline. In addition, tissues which may be treated by the system and method of the present invention further include, but are not limited to, tissues of the heart, chest, knee, shoulder, ankle, hip, elbow, hand or foot; as well as prostate
25 tissue, leiomyomas (fibroids) located within the uterus, gingival tissues and mucosal tissues located in the mouth, tumors, scar tissue, myocardial tissue, collagenous tissue within the eye; together with epidermal and dermal tissues on the surface of the skin. The present invention is also useful for resecting tissue within accessible sites of the body that are suitable for electrode loop resection, such as the resection
30 of prostate tissue, leiomyomas (fibroids) located within the uterus, or other tissue to be removed from the body.

The present invention is also useful for procedures in the head and neck, such as the ear, mouth, throat, pharynx, larynx, esophagus, nasal cavity, and sinuses. These procedures may be performed through the mouth or nose using speculae or gags, or using endoscopic techniques, such as functional endoscopic sinus surgery (FESS). These procedures may include the removal of swollen tissue, chronically-diseased inflamed and hypertrophic mucous linings, polyps and/or neoplasms from the various anatomical sinuses of the skull, the turbinates and nasal passages, in the tonsil, adenoid, epi-glottic and supra-glottic regions, and salivary glands, submucous resection of the nasal septum, excision of diseased tissue and the like. In other procedures, the present invention may be useful for cutting, resection, ablation and/or hemostasis of tissue in procedures for treating snoring and obstructive sleep apnea (e.g., UPPP procedures), for gross tissue removal, such as tonsillectomies, adenoidectomies, tracheal stenosis and vocal cord polyps and lesions, or for the resection or ablation of facial tumors or tumors within the mouth and pharynx, such as glossectomies, laryngectomies, acoustic neuroma procedures and nasal ablation procedures. In addition, the present invention is useful for procedures within the ear, such as stapedotomies, tympanostomies, myringotomies, or the like.

The present invention may also be useful for cosmetic and plastic surgery procedures in the head and neck. For example, the present invention is particularly useful for ablation and sculpting of cartilage tissue, such as the cartilage within the nose that is sculpted during rhinoplasty procedures. The present invention may also be employed for skin tissue removal and/or collagen shrinkage in the epidermis or dermis tissue in the head and neck region, e.g., the removal of pigmentations, vascular lesions, scars, tattoos, etc., and for other surgical procedures on the skin, such as tissue rejuvenation, cosmetic eye procedures (blepharoplasties), wrinkle removal, tightening muscles for facelifts or browlifts, hair removal and/or transplant procedures, etc.

The present invention is also useful for harvesting blood vessels, such as a blood vessel to be used as a graft vessel during the CABG procedure, e.g., the saphenous vein and the internal mammary artery (IMA). One or more embodiments of the invention may be used as follows: i) to access the blood vessel to be

harvested, e.g., by opening the leg to access the saphenous vein, or opening the chest (either via a longitudinal incision of the sternum during an open-chest procedure, or during a minimally invasive inter-costal procedure); ii) to dissect the blood vessel to be harvested from the surrounding connective tissue along at least a portion of its length; and iii) to transect the dissected blood vessel at a first position only in the case of a pedicled graft (IMA), or at the first position and at a second position in the case of a free graft (saphenous vein). In each case i) to iii), as well as for other embodiment of the invention, the procedure involves removal of tissue by a cool ablation procedure in which a high frequency voltage is applied to an active electrode in the vicinity of a target tissue, typically in the presence of an electrically conductive fluid. The cool ablation procedure of the invention is described fully elsewhere herein. The electrically conductive fluid may be a bodily fluid such as blood or synovial fluid, intracellular fluid of the target tissue, or isotonic saline delivered to the target tissue during the procedure. The present invention is also useful for coagulating blood or blood vessels, for example, to minimize bleeding in the sternum during an open-chest procedure.

Although certain parts of this disclosure are directed specifically to creating incisions for accessing a patient's thoracic cavity and the harvesting and dissection of blood vessels within the body during a CABG procedure, systems and methods of the invention are equally applicable to other procedures involving other organs or tissues of the body, including minimally invasive procedures (e.g., minimally invasive CABG procedures), other open procedures, intravascular procedures, urological procedures, laparoscopy, arthroscopy, thoracoscopy or other cardiac procedures, cosmetic surgery, orthopedics, gynecology, otorhinolaryngology, spinal and neurologic procedures, oncology, and the like.

In methods of the present invention, high frequency (RF) electrical energy is usually applied to one or more active electrodes in the presence of an electrically conductive fluid to remove and/or modify target tissue, an organ, or a body structure. Depending on the specific procedure, the present invention may be used to: (1) create incisions in tissue; (2) dissect or harvest tissue; (3) volumetrically remove tissue or cartilage (i.e., ablate or effect molecular dissociation of the tissue); (4) cut, transect, or resect tissue or an organ (e.g., a blood vessel); (5) create

perforations or holes within tissue; and/or (6) coagulate blood and severed blood vessels.

In one method of the present invention, the tissue structures are incised by volumetrically removing or ablating tissue along a cutting path. In this procedure, a high frequency voltage difference is applied between one or more active electrode (s) and one or more return electrode(s) to develop high electric field intensities in the vicinity of the target tissue site. The high electric field intensities lead to electric field induced molecular breakdown of target tissue through molecular dissociation (rather than thermal evaporation or carbonization). Applicant believes that the tissue structure is volumetrically removed through molecular disintegration of larger organic molecules into smaller molecules and/or atoms, such as hydrogen, oxides of carbon, hydrocarbons and nitrogen compounds. This molecular disintegration completely removes the tissue structure, as opposed to dehydrating the tissue material by the removal of liquid within the cells of the tissue, as is typically the case with electrosurgical desiccation and vaporization.

The high electric field intensities may be generated by applying a high frequency voltage that is sufficient to vaporize an electrically conductive fluid over at least a portion of the active electrode(s) in the region between the tip of the active electrode(s) and the target tissue. The electrically conductive fluid may be a gas or liquid, such as isotonic saline, delivered to the target site, or a viscous fluid, such as a gel, that is located at the target site. In the latter embodiment, the active electrode(s) are submersed in the electrically conductive gel during the surgical procedure. Since the vapor layer or vaporized region has a relatively high electrical impedance, it minimizes the current flow into the electrically conductive fluid. Within the vaporized fluid a plasma is formed, and charged particles (e.g., electrons) cause the localized molecular dissociation or disintegration of components of the target tissue, to a depth of perhaps several cell layers. This molecular dissociation results in the volumetric removal of tissue from the target site. This ablation process, which typically subjects the target tissue to a temperature in the range of 40° C to 70° C, can be precisely controlled to effect the removal of tissue to a depth as little as about 10 microns, with little or no thermal or other damage to surrounding tissue. This cool ablation phenomenon has been termed Coblation®.

While not being bound by theory, applicant believes that the principle mechanism of tissue removal in the Coblation[®] mechanism of the present invention is energetic electrons or ions that have been energized in a plasma adjacent to the active electrode(s). When a liquid is heated sufficiently that atoms vaporize from the liquid at a greater rate than they recondense, a gas is formed. When the gas is heated sufficiently that the atoms collide with each other and electrons are removed from the atoms in the process, an ionized gas or plasma is formed. (A more complete description of plasmas (the so-called "fourth state of matter") can be found in Plasma Physics, by R.J. Goldston and P.H. Rutherford of the Plasma Physics Laboratory of Princeton University (1995), the complete disclosure of which is incorporated herein by reference.) When the density of the vapor layer (or within a bubble formed in the electrically conductive liquid) becomes sufficiently low (i.e., less than approximately 10^{20} atoms/cm³ for aqueous solutions), the electron mean free path increases to enable subsequently injected electrons to cause impact ionization within these regions of low density (i.e., vapor layers or bubbles). Once the ionic particles in the plasma layer have sufficient energy, they accelerate towards the target tissue. Energy evolved by the energetic electrons (e.g., 3.5 eV to 5 eV) can subsequently bombard a molecule and break its bonds, dissociating a molecule into free radicals, which then combine into final gaseous or liquid species.

Plasmas may be formed by heating and ionizing a gas by driving an electric current through it, or by transmitting radio waves into the gas. Generally, these methods of plasma formation give energy to free electrons in the plasma directly, and then electron-atom collisions liberate more electrons, and the process cascades until the desired degree of ionization is achieved. Often, the electrons carry the electrical current or absorb the radio waves and, therefore, are hotter than the ions. Thus, in applicant's invention, the electrons, which are carried away from the tissue towards the return electrode, carry most of the plasma's heat with them, allowing the ions to break apart the tissue molecules in a substantially non-thermal manner.

The energy evolved by the energetic electrons may be varied by adjusting a variety of factors, such as: the number of active electrodes; electrode

size and spacing; electrode surface area; asperities and sharp edges on the electrode surfaces; electrode materials; applied voltage and power; current limiting means, such as inductors; electrical conductivity of the fluid in contact with the electrodes; density of the fluid; electrical insulators over the electrodes; and other factors.

- 5 Accordingly, these factors can be manipulated to control the energy level of the excited electrons. Since different tissue structures have different molecular bonds, the present invention can be configured to break the molecular bonds of certain tissue, while having too low an energy to break the molecular bonds of other tissue. For example, fatty tissue, (e.g., adipose tissue) contains a large amount of lipid
- 10 material having double bonds, the breakage of which requires an energy level substantially higher than 4 eV to 5 eV. Accordingly, the present invention can be configured such that lipid components of adipose tissue are selectively not ablated. Of course, the present invention may be used to effectively ablate cells of adipose tissue such that the inner fat content of the cells is released in a liquid form.
- 15 Alternatively, the invention can be configured (e.g., by increasing the voltage or changing the electrode configuration to increase the current density at the electrode tips) such that the double bonds of lipid materials are readily broken leading to molecular dissociation of lipids into low molecular weight condensable gases, generally as described hereinabove. A more complete description of the Coblation[®]
- 20 phenomenon can be found in commonly assigned U.S. Patent No. 5,683,366 and co-pending U.S. Patent Application 09/032,375, filed February 27, 1998 (Attorney Docket No. CB-3), the complete disclosures of which are incorporated herein by reference.

- 25 Methods of the present invention typically involve the application of high frequency (RF) electrical energy to one or more active electrodes in the presence of an electrically conductive fluid to remove (i.e., resect, incise, perforate, cut, or ablate) a target tissue, structure, or organ; and/or to seal transected vessels within the region of the target tissue. The present invention is particularly useful for sealing larger arterial vessels, e.g., having a diameter on the order of 1 mm or
- 30 greater. In some embodiments, a high frequency power supply is provided having an ablation mode, wherein a first voltage is applied to an active electrode sufficient to effect molecular dissociation or disintegration of the tissue; and a coagulation

mode, wherein a second, lower voltage is applied to an active electrode (either the same or a different electrode) sufficient to achieve hemostasis of severed vessels within the tissue. In other embodiments, an electrosurgical probe is provided having one or more coagulation electrode(s) configured for sealing a severed vessel, such as an arterial vessel, and one or more active electrodes configured for either contracting the collagen fibers within the tissue or removing (ablating) the tissue, e.g., by applying sufficient energy to the tissue to effect molecular dissociation. In the latter embodiments, the coagulation electrode(s) may be configured such that a single voltage can be applied to both coagulate with the coagulation electrode(s), and to ablate or contract tissue with the active electrode(s). In other embodiments, the power supply is combined with the coagulation probe such that the coagulation electrode is used when the power supply is in the coagulation mode (low voltage), and the active electrode(s) are used when the power supply is in the ablation mode (higher voltage).

In one method of the present invention, one or more active electrodes are brought into close proximity to tissue at a target site, and the power supply is activated in the ablation mode such that sufficient voltage is applied between the active electrodes and the return electrode to volumetrically remove the tissue through molecular dissociation, as described above. During this process, vessels within the tissue are severed. Smaller vessels may be automatically sealed with the system and method of the present invention. Larger vessels and those with a higher flow rate, such as arterial vessels, may not be automatically sealed in the ablation mode. In these cases, the severed vessels may be sealed by actuating a control (e.g., a foot pedal) to reduce the voltage of the power supply into the coagulation mode. In this mode, the active electrodes may be pressed against the severed vessel to provide sealing and/or coagulation of the vessel. Alternatively, a coagulation electrode located on the same or a different probe may be pressed against the severed vessel. Once the vessel is adequately sealed, the surgeon may activate a control (e.g., another foot pedal) to increase the voltage of the power supply back into the ablation mode.

The present invention is also useful for removing or ablating tissue around nerves, such as spinal, or cranial nerves, e.g., the hypoglossal nerve, the

optic nerve, facial nerves, vestibulocochlear nerves and the like. This is particularly advantageous when removing tissue that is located close to nerves. One of the significant drawbacks with the conventional RF devices, scalpels, and lasers is that these devices do not differentiate between the target tissue and the surrounding nerves or bone. Therefore, the surgeon must be extremely careful during these procedures to avoid damage to the nerves within and around the target tissue. In the present invention, the Coblation® process for removing tissue results in no, or extremely small amounts, of collateral tissue damage, as described above. This allows the surgeon to remove tissue close to a nerve without causing collateral damage to the nerve fibers and surrounding tissue.

In addition to the generally precise nature of the novel mechanisms of the present invention, applicant has discovered an additional method of ensuring that adjacent nerves are not damaged during tissue removal. According to the present invention, systems and methods are provided for distinguishing between the fatty tissue immediately surrounding nerve fibers and the normal tissue that is to be removed during the procedure. Peripheral nerves usually comprise a connective tissue sheath, or epineurium, enclosing the bundles of nerve fibers, each bundle being surrounded by its own sheath of connective tissue (the perineurium) to protect these nerve fibers. The outer protective tissue sheath or epineurium typically comprises a fatty tissue (e.g., adipose tissue) having substantially different electrical properties than the normal target tissue that is treated. The system of the present invention measures the electrical properties of the tissue at the tip of the probe with one or more active electrode(s). These electrical properties may include electrical conductivity at one, several, or a range of frequencies (e.g., in the range from 1 kHz to 100 MHz), dielectric constant, capacitance or combinations of these. In this embodiment, an audible signal may be produced when the sensing electrode(s) at the tip of the probe detects the fatty tissue surrounding a nerve, or direct feedback control can be provided to only supply power to the active electrode(s) either individually or to the complete array of electrodes, if and when the tissue encountered at the tip or working end of the probe is normal tissue based on the measured electrical properties.

In one embodiment, the current limiting elements are configured such that the active electrodes will shut down or turn off when the electrical impedance reaches a threshold level. When this threshold level is set to the impedance of the fatty tissue surrounding nerves, the active electrodes will shut off whenever they come in contact with, or in close proximity to, nerves. Meanwhile, the other active electrodes, which are in contact with or in close proximity to target tissue, will continue to conduct electric current to the return electrode. This selective ablation or removal of lower impedance tissue in combination with the Coblation[®] mechanism of the present invention allows the surgeon to precisely remove tissue around nerves or bone. Applicant has found that the present invention is capable of volumetrically removing tissue closely adjacent to nerves without impairing the function of the nerves, and without significantly damaging the tissue of the epineurium.

The present invention can be also be configured to create an incision in a bone of the patient. For example, the systems of the present invention can be used to create an incision in the sternum for access to the thoracic cavity. Applicant has found that the Coblation[®] mechanism of the present invention allows the surgeon to precisely create an incision in the sternum while minimizing or preventing bone bleeding. The high frequency voltage is applied between the active electrode(s) and the return electrode(s) to volumetrically remove the bone from a specific site targeted for the incision. As the active electrode(s) are passed through the incision in the bone, the sides of the active electrodes (or a third coagulation electrode) slidingly contact the bone surrounding the incision to provide hemostasis in the bone. A more complete description of such coagulation electrodes can be found in U.S. Patent Application Serial No. 09/162,117, filed September 28, 1998, the complete disclosure of which is incorporated herein by reference.

The present invention can also be used to dissect and harvest blood vessels from the patient's body during a CABG procedure. The system of the present invention allows a surgeon to dissect and harvest blood vessels, such as the right or left IMA or saphenous vein, while concurrently providing hemostasis at the harvesting site. In some embodiments, a first high frequency voltage, can be delivered in an ablation mode to effect molecular disintegration of connective tissue

adjacent to the blood vessel targeted for harvesting; and a second, lower voltage can be delivered to achieve hemostasis of the connective tissue adjacent to the blood vessel. In other embodiments, the targeted blood vessel can be transected at one or more positions along its length, and one or more coagulation electrode(s) can be used to seal the transected blood vessel at the site of transection. The coagulation electrode(s) may be configured such that a single voltage can be applied to the active electrodes to ablate the tissue and to coagulate the blood vessel and target site.

The present invention also provides systems, apparatus, and methods for selectively removing tumors or other undesirable body structures while minimizing the spread of viable cells from the tumor. Conventional techniques for removing such tumors generally result in the production of smoke in the surgical setting, termed an electrosurgical or laser plume, which can spread intact, viable bacterial or viral particles from the tumor or lesion to the surgical team, or viable cancerous cells to other locations within the patient's body. This potential spread of viable cells or particles has resulted in increased concerns over the proliferation of certain debilitating and fatal diseases, such as hepatitis, herpes, HIV, and papillomavirus. In the present invention, high frequency voltage is applied between the active electrode(s) and one or more return electrode(s) to volumetrically remove at least a portion of the tissue cells in the tumor or lesion by the molecular dissociation of tissue components into non-condensable gases. The high frequency voltage is preferably selected to effect controlled removal of these tissue cells while minimizing substantial tissue necrosis to surrounding or underlying tissue. A more complete description of this phenomenon can be found in co-pending U.S. Patent Application 09/109,219, filed June 30, 1998 (Attorney Docket No. CB-1), the complete disclosure of which is incorporated herein by reference.

A current flow path between the active electrode(s) and the return electrode(s) may be generated by submerging the tissue site in an electrically conductive fluid (e.g., within a viscous fluid, such as an electrically conductive gel) or by directing an electrically conductive fluid along a fluid path to the target site (i.e., a liquid, such as isotonic saline, or a gas, such as argon). This latter method is particularly effective in a dry field procedure (i.e., the tissue is not submersed in fluid). The use of a conductive gel allows a slower, more controlled delivery rate of

conductive fluid as compared with a liquid or a gas. In addition, the viscous nature of the gel may allow the surgeon to more easily contain the gel around the target site (e.g., as compared with containment of isotonic saline). A more complete description of an exemplary method of directing electrically conductive fluid between the active and return electrodes is described in U.S. Patent No. 5,697,281, the full disclosure of which is incorporated herein by reference. Alternatively, the body's natural conductive fluids, such as blood, may be sufficient to establish a conductive path between the return electrode(s) and the active electrode(s), and to provide the conditions for establishing a vapor layer, as described above. However, conductive fluid that is introduced into the patient is generally preferred over blood because blood will tend to coagulate at certain temperatures. Advantageously, a liquid electrically conductive fluid (e.g., isotonic saline) may be used to concurrently "bathe" the target tissue surface to provide an additional means for removing any tissue, and to cool the tissue at or adjacent to the target site.

In some embodiments of the invention, an electrosurgical probe includes an electrode support for electrically isolating the active electrode(s) from the return electrode, and a fluid delivery port or outlet for directing an electrically conductive fluid to the target site or to the distal end of the probe. The electrode support and the fluid outlet may be recessed from an outer surface of the instrument to confine the electrically conductive fluid to the region immediately surrounding the electrode support. In addition, a shaft of the instrument may be shaped so as to form a cavity around the electrode support and the fluid outlet. This helps to assure that the electrically conductive fluid will remain in contact with the active electrode(s) and the return electrode(s) to maintain the conductive path therebetween. In addition, this will help to maintain a vapor layer and subsequent plasma layer between the active electrode(s) and the tissue at the treatment site throughout the procedure, thereby reducing any thermal damage that might otherwise occur if the vapor layer were extinguished due to a lack of conductive fluid. Provision of the electrically conductive fluid around the target site also helps to maintain the tissue temperature at desired levels.

The electrically conductive fluid should have a threshold conductivity to provide a suitable conductive path between the return electrode and the active

electrode(s). The electrical conductivity of the fluid (in units of milliSiemens per centimeter or mS/cm) will usually be greater than 0.2 mS/cm, preferably will be greater than 2 mS/cm and more preferably greater than 10 mS/cm. In an exemplary embodiment, the electrically conductive fluid is isotonic saline, which has a conductivity of about 17 mS/cm.

An electrosurgical probe or instrument of the invention typically includes a shaft having a proximal end and a distal end, and one or more active electrode(s) disposed at the shaft distal end. The shaft serves to mechanically support the active electrode(s) and permits the treating physician to manipulate the shaft distal end via a handle attached to the proximal end of the shaft. The shaft may be rigid or flexible, with flexible shafts optionally being combined with a generally rigid external tube for mechanical support. Flexible shafts may be combined with pull wires, shape memory actuators, and other known mechanisms for effecting selective deflection of the distal end of the shaft to facilitate positioning of the electrode array. The shaft will usually have one or more wires, electrode connectors, leads, or other conductive elements running axially therethrough, to permit connection of the electrode(s) to a connection block located at the proximal end of the instrument. The connection block is adapted for coupling the electrode(s) to the power supply or controller. Typically, the connection block is housed within the handle of the probe.

The shaft of an instrument under the invention may assume various configurations. Generally, the shaft will have a suitable diameter and length to allow the surgeon to access the target site with the distal or working end of the shaft. Thus, the shaft may be provided in a range of sizes according to the particular procedure or tissue targeted for treatment. Typically, the shaft will have a length in the range of from about 5 cm to 30 cm, and have a diameter in the range of from about 0.5 mm to 10 mm. Specific shaft designs will be described in detail in connection with the drawings hereinafter.

The present invention may use a single active electrode or a plurality of electrodes distributed across a contact surface of a probe (e.g., in a linear fashion). In the latter embodiment, the electrode array usually includes a plurality of independently current-limited and/or power-controlled active electrodes to apply

electrical energy selectively to the target tissue while limiting the unwanted application of electrical energy to the surrounding tissue and environment resulting from power dissipation into surrounding electrically conductive liquids, such as blood, normal saline, electrically conductive gel and the like. The active electrodes may be independently current-limited by isolating the terminals from each other and connecting each terminal to a separate power source that is isolated from the other active electrodes. Alternatively, the active electrodes may be connected to each other at either the proximal or distal ends of the probe to form a single wire that couples to a power source.

In one configuration, each individual active electrode is electrically insulated from all other active electrodes within the probe and is connected to a power source which is isolated from each of the other active electrodes in the array, or to circuitry which limits or interrupts current flow to the active electrode when low resistivity material causes a low impedance path between the return electrode and the individual active electrode. The isolated power sources for each individual active electrode may be separate power supply circuits having internal impedance characteristics which limit power to the associated active electrode when a low impedance return path is encountered. By way of example, the isolated power source may be a user selectable constant current source. In this embodiment, lower impedance paths will automatically result in lower resistive heating levels since the heating is proportional to the square of the operating current times the impedance. Alternatively, a single power source may be connected to each of the active electrodes through independently actuatable switches, or by independent current limiting elements, such as inductors, capacitors, resistors and/or combinations thereof. The current limiting elements may be provided in the probe, connectors, cable, power supply or along the conductive path from the power supply to the distal tip of the probe. Alternatively, the resistance and/or capacitance may occur on the surface of the active electrode(s) due to oxide layers which form selected active electrodes (e.g., titanium or a resistive coating on the surface of metal, such as platinum).

The distal end of the probe may comprise many independent active electrodes designed to deliver electrical energy in the vicinity of the distal end. The

selective application of electrical energy to the conductive fluid is achieved by connecting each individual active electrode and the return electrode to a power source having independently controlled or current limited channels. The return electrode(s) may comprise a single tubular member of electrically conductive material at the distal end of the probe proximal to the active electrode(s). The same tubular member of electrically conductive material may also serve as a conduit for the supply of the electrically conductive fluid between the active and return electrodes. The application of high frequency voltage between the return electrode(s) and the active electrode(s) results in the generation of high electric field intensities at the distal tip of the active electrode(s), with conduction of high frequency current from each active electrode to the return electrode. The current flow from each active electrode to the return electrode(s) is controlled by either active or passive means, or a combination thereof, to deliver electrical energy to the surrounding conductive fluid while minimizing energy delivery to surrounding (non-target) tissue.

The application of a suitable high frequency voltage between the return electrode(s) and the active electrode(s) for appropriate time intervals effects cutting, removing, ablating, shaping, contracting or otherwise modifying the target tissue. In one embodiment, the tissue volume over which energy is dissipated (*i.e.*, over which a high current density exists) may be precisely controlled, for example, by the use of a multiplicity of small active electrodes whose effective diameters or principal dimensions range from about 5 mm to 0.01 mm, preferably from about 2 mm to 0.05 mm, and more preferably from about 1 mm to 0.1 mm. Electrode areas for both circular and non-circular terminals will have a contact area (per active electrode) below 25 mm², preferably being in the range from 0.0001 mm² to 1 mm², and more preferably from 0.005 mm² to .5 mm². The circumscribed area of the electrode array is in the range from 0.25 mm² to 75 mm², preferably from 0.5 mm² to 40 mm². In one embodiment the probe may include a plurality of relatively small active electrodes disposed over the distal contact surfaces on the shaft. The use of small diameter active electrodes increases the electric field intensity and reduces the extent or depth of tissue heating as a consequence of the divergence of current flux lines which emanate from the exposed surface of each active electrode.

The portion of the electrode support on which the active electrode(s) are mounted generally defines a tissue treatment surface of the probe. The area of the tissue treatment surface can vary widely, and the tissue treatment surface can assume a variety of geometries, with particular areas and geometries being selected for specific applications. The area of the tissue treatment surface can range from about 0.25 mm² to 75 mm², usually being from about 0.5 mm² to 40 mm². The geometries of the active electrode(s) can be planar, concave, convex, hemispherical, conical, a linear "in-line" array, or virtually any other regular or irregular shape. Most commonly, the active electrode(s) will be located at the shaft distal end of the electrosurgical probe, frequently having planar, disk-shaped, or hemispherical surfaces for use in reshaping procedures, ablating, cutting, dissecting organs, coagulating, or transecting blood vessels. The active electrode(s) may be arranged terminally or laterally on the electrosurgical probe (e.g., in the manner of a scalpel or a blade). However, it should be clearly understood that the active electrode of the invention does not cut or sever tissue mechanically as for a scalpel blade, but rather by the localized molecular dissociation of tissue components due to application of high frequency electric current to the active electrode. In one embodiment, a distal portion of the shaft may be flattened or compressed laterally (e.g., Figs. 32A-32C). A probe having a laterally compressed shaft may facilitate access to certain target sites or body structures during various surgical procedures.

In embodiments having a plurality of active electrodes, it should be clearly understood that the invention is not limited to electrically isolated active electrodes. For example, a plurality of active electrodes may be connected to a single lead that extends through the probe shaft and is coupled to a high frequency power supply. Alternatively, the probe may incorporate a single electrode that extends directly through the probe shaft or is connected to a single lead that extends to the power source. The active electrode may have a planar or blade shape, a screwdriver or conical shape, a sharpened point, a ball shape (e.g., for tissue vaporization and desiccation), a twizzle shape (for vaporization and needle-like cutting), a spring shape (for rapid tissue debulking and desiccation), a twisted metal shape, an annular or solid tube shape, or the like. Alternatively, the electrode may comprise a plurality of filaments, a rigid or flexible brush electrode (for debulking a

tumor, such as a fibroid, bladder tumor or a prostate adenoma), a side-effect brush electrode on a lateral surface of the shaft, a coiled electrode, or the like.

In one embodiment, the probe comprises a single blade active electrode that extends from an insulating support member, spacer, or electrode support, e.g., a ceramic or silicone rubber spacer located at the distal end of the probe. The insulating support member may be a tubular structure or a laterally compressed structure that separates the blade active electrode from a tubular or annular return electrode positioned proximal to the insulating member and the active electrode. The blade electrode may include a distal cutting edge and sides which are configured to coagulate the tissue as the blade electrode advances through the tissue. In yet another embodiment, the catheter or probe includes a single active electrode that can be rotated relative to the rest of the catheter body, or the entire catheter may be rotated relative to the electrode lead(s). The single active electrode can be positioned adjacent the abnormal tissue and energized and rotated as appropriate to remove or modify the target tissue.

The active electrode(s) are preferably supported within or by an insulating support member positioned near the distal end of the instrument shaft. The return electrode may be located on the instrument shaft, on another instrument, or on the external surface of the patient (i.e., a dispersive pad). For certain procedures, the close proximity of nerves and other sensitive tissue makes a bipolar design more preferable because this minimizes the current flow through non-target tissue and surrounding nerves. Accordingly, the return electrode is preferably either integrated with the instrument body, or located on another instrument. The proximal end of the probe typically includes the appropriate electrical connections for coupling the return electrode(s) and the active electrode(s) to a high frequency power supply, such as an electrosurgical generator.

One exemplary power supply of the present invention delivers a high frequency current selectable to generate average power levels ranging from several milliwatts to tens of watts per electrode, depending on the volume of target tissue being treated, and/or the maximum allowed temperature selected for the instrument tip. The power supply allows the user to select the voltage level according to the specific requirements of a particular otologic procedure, neurosurgery procedure,

cardiac surgery, arthroscopic surgery, dermatological procedure, ophthalmic procedures, open surgery or other endoscopic surgery procedure. For cardiac procedures and potentially for neurosurgery, the power source may have an additional filter, for filtering leakage voltages at frequencies below 100 kHz, particularly voltages around 60 kHz. Alternatively, a power supply having a higher operating frequency, e.g., 300 kHz to 500 kHz may be used in certain procedures in which stray low frequency currents may be problematic. A description of one suitable power supply can be found in co-pending Patent Applications 09/058,571 and 09/058,336, filed April 10, 1998 (Attorney Docket Nos. CB-2 and CB-4), the complete disclosure of both applications are incorporated herein by reference for all purposes.

The voltage difference applied between the return electrode(s) and the active electrode(s) will be at high or radio frequency, typically between about 5 kHz and 20 MHz, usually being between about 30 kHz and 2.5 MHz, preferably being between about 50 kHz and 500 kHz, often less than 350 kHz, and often between about 100 kHz and 200 kHz. The RMS (root mean square) voltage applied will usually be in the range from about 5 volts to 1000 volts, preferably being in the range from about 10 volts to 500 volts depending on the active electrode size, the operating frequency, and the operation mode of the particular procedure or desired effect on the tissue (e.g., contraction, coagulation, cutting or ablation). Typically, the peak-to-peak voltage for ablation or cutting will be in the range of 10 volts to 2000 volts and preferably in the range of 200 volts to 1800 volts, and more preferably in the range of about 300 volts to 1500 volts, often in the range of about 500 volts to 900 volts peak to peak (again, depending on the electrode size, the operating frequency and the operation mode). Lower peak-to-peak voltages will be used for tissue coagulation or collagen contraction and will typically be in the range from 50 to 1500, preferably 100 to 1000, and more preferably 120 to 600 volts peak-to-peak.

The voltage is usually delivered in a series of voltage pulses or alternating current of time varying voltage amplitude with a sufficiently high frequency (e.g., on the order of 5 kHz to 20 MHz) such that the voltage is effectively applied continuously (as compared with e.g., lasers claiming small

depths of necrosis, which are generally pulsed about 10 Hz to 20 Hz). In addition, the duty cycle (i.e., cumulative time in any one-second interval that energy is applied) is on the order of about 50% for the present invention, as compared with pulsed lasers which typically have a duty cycle of about 0.0001%.

5 The power supply may include a fluid interlock for interrupting power to the active electrode(s) when there is insufficient conductive fluid around the active electrode(s). This ensures that the instrument will not be activated when conductive fluid is not present, minimizing the tissue damage that may otherwise occur. A more complete description of such a fluid interlock can be found in
10 commonly assigned, co-pending U.S. Application No. 09/058,336, filed April 10, 1998 (attorney Docket No. CB-4), the complete disclosure of which is incorporated herein by reference.

 The power supply may also be current limited or otherwise controlled so that undesired heating of the target tissue or surrounding (non-target) tissue does
15 not occur. In a presently preferred embodiment of the present invention, current limiting inductors are placed in series with each independent active electrode, where the inductance of the inductor is in the range of 10uH to 50,000uH, depending on the electrical properties of the target tissue, the desired tissue heating rate and the operating frequency. Alternatively, capacitor-inductor (LC) circuit structures may
20 be employed, as described previously in U.S. Patent No. 5,697,909, the complete disclosure of which is incorporated herein by reference. Additionally, current limiting resistors may be selected. Preferably, these resistors will have a large positive temperature coefficient of resistance so that, as the current level begins to rise for any individual active electrode in contact with a low resistance medium
25 (e.g., saline irrigant or blood), the resistance of the current limiting resistor increases significantly, thereby minimizing the power delivery from the active electrode into the low resistance medium (e.g., saline irrigant or blood).

 In some procedures, it may also be necessary to retrieve or aspirate the electrically conductive fluid and/or the non-condensable gaseous products of
30 ablation. In addition, it may be desirable to aspirate small pieces of tissue or other body structures that are not completely disintegrated by the high frequency energy, or other fluids at the target site, such as blood, mucus, purulent fluid, the gaseous

products of ablation, or the like. Accordingly, the system of the present invention may include one or more suction lumen(s) in the instrument, or on another instrument, coupled to a suitable vacuum source for aspirating fluids from the target site. In addition, the invention may include one or more aspiration electrode(s) coupled to the distal end of the suction lumen for ablating, or at least reducing the volume of, non-ablated tissue fragments that are aspirated into the lumen. The aspiration electrode(s) function mainly to inhibit clogging of the lumen that may otherwise occur as larger tissue fragments are drawn therein. The aspiration electrode(s) may be different from the ablation active electrode(s), or the same electrode(s) may serve both functions. A more complete description of instruments incorporating aspiration electrode(s) can be found in commonly assigned, co-pending patent Application No. 09/010,382, filed January 21, 1998, the complete disclosure of which is incorporated herein by reference.

During a surgical procedure, the distal end of the instrument and the active electrode(s) may be maintained at a small distance away from the target tissue surface. This small spacing allows for the continuous flow of electrically conductive fluid into the interface between the active electrode(s) and the target tissue surface. The continuous flow of the electrically conductive fluid helps to ensure that the thin vapor layer will remain between the active electrode(s) and the tissue surface. In addition, dynamic movement of the active electrode(s) over the tissue site allows the electrically conductive fluid to cool the tissue underlying and surrounding the target tissue to minimize thermal damage to this surrounding and underlying tissue. Accordingly, the electrically conductive fluid may be cooled to facilitate the cooling of the tissue. Typically, the active electrode(s) will be about 0.02 mm to 2 mm from the target tissue and preferably about 0.05 mm to 0.5 mm during the ablation process. One method of maintaining this space is to move, translate and/or rotate the probe transversely relative to the tissue, i.e., for the operator to use a light brushing motion, to maintain a thin vaporized layer or region between the active electrode and the tissue. Of course, if coagulation or collagen shrinkage of a deeper region of tissue is necessary (e.g., for sealing a bleeding vessel embedded within the tissue), it may be desirable to press the active electrode(s) against the tissue to effect joulean heating therein.

Referring to Fig. 1, an exemplary electrosurgical system 11 for cutting, ablating, resecting, or otherwise modifying tissue will now be described in detail. Electrosurgical system 11 generally comprises an electrosurgical handpiece or probe 10 connected to a power supply 28 for providing high frequency voltage to a target site, and a fluid source 21 for supplying electrically conductive fluid 50 to, probe 10. In addition, electrosurgical system 11 may include an endoscope (not shown) with a fiber optic head light for viewing the surgical site. The endoscope may be integral with probe 10, or it may be part of a separate instrument. The system 11 may also include a vacuum source (not shown) for coupling to a suction lumen or tube 211 (see Fig. 2) in the probe 10 for aspirating the target site.

As shown, probe 10 generally includes a proximal handle 19 and an elongate shaft 18 having one or more active electrodes 58 at its distal end. A connecting cable 34 has a connector 26 for electrically coupling the active electrodes 58 to power supply 28. In embodiments having a plurality of active electrodes, active electrodes 58 are electrically isolated from each other and the terminal of each active electrode 58 is connected to an active or passive control network within power supply 28 by means of a plurality of individually insulated conductors (not shown). A fluid supply tube 15 is connected to a fluid tube 14 of probe 10 for supplying electrically conductive fluid 50 to the target site.

Power supply 28 has an operator controllable voltage level adjustment 30 to change the applied voltage level, which is observable at a voltage level display 32. Power supply 28 also includes first, second, and third foot pedals 37, 38, 39 and a cable 36 which is removably coupled to power supply 28. The foot pedals 37, 38, 39 allow the surgeon to remotely adjust the energy level applied to active electrode(s) 58. In an exemplary embodiment, first foot pedal 37 is used to place the power supply into the "ablation" mode and second foot pedal 38 places power supply 28 into the "coagulation" mode. The third foot pedal 39 allows the user to adjust the voltage level within the ablation mode. In the ablation mode, a sufficient voltage is applied to the active electrodes to establish the requisite conditions for molecular dissociation of the tissue (i.e., vaporizing a portion of the electrically conductive fluid, ionizing the vapor layer and accelerating charged particles against the tissue). As discussed above, the requisite voltage level for ablation will vary

depending on the number, size, shape and spacing of the electrodes, the distance in which the electrodes extend from the support member, etc. When the surgeon is using the power supply in the ablation mode, voltage level adjustment 30 or third foot pedal 39 may be used to adjust the voltage level to adjust the degree or aggressiveness of the ablation.

Of course, it will be recognized that the voltage and modality of the power supply may be controlled by other input devices. However, applicant has found that foot pedals are convenient means for controlling the power supply while manipulating the probe during a surgical procedure.

In the coagulation mode, the power supply 28 applies a low enough voltage to the active electrode(s) (or the coagulation electrode) to avoid vaporization of the electrically conductive fluid and subsequent molecular dissociation of the tissue. The surgeon may automatically switch the power supply between the ablation and coagulation modes by alternately stepping on foot pedals 37, 38, respectively. This allows the surgeon to quickly move between coagulation and ablation *in situ*, without having to remove his/her concentration from the surgical field or without having to request an assistant to switch the power supply. By way of example, as the surgeon is sculpting soft tissue in the ablation mode, the probe typically will simultaneously seal and/or coagulation small severed vessels within the tissue. However, larger vessels, or vessels with high fluid pressures (e.g., arterial vessels) may not be sealed in the ablation mode. Accordingly, the surgeon can simply step on foot pedal 38, automatically lowering the voltage level below the threshold level for ablation, and apply sufficient pressure onto the severed vessel for a sufficient period of time to seal and/or coagulate the vessel. After this is completed, the surgeon may quickly move back into the ablation mode by stepping on foot pedal 37. A specific design of a suitable power supply for use with the present invention can be found in Provisional Patent Application No. 60/062,997, filed October 23, 1997 (Attorney Docket No. 16238-007400), previously incorporated herein by reference.

Fig. 2 shows an electrosurgical probe 20 according to one embodiment of the invention. Probe 20 may be used in conjunction with a system similar or analogous to system 11 (Fig. 1). As shown in Fig. 2, probe 20 generally

includes an elongated shaft 100 which may be flexible or rigid, a handle 204 coupled to the proximal end of shaft 100 and an electrode support member 102 coupled to the distal end of shaft 100. Shaft 100 may comprise a plastic material that is easily molded into the shape shown in Fig. 3, or shaft 100 may comprise an electrically conducting material, usually a metal, such as tungsten, stainless steel alloys, platinum or its alloys, titanium or its alloys, molybdenum or its alloys, and nickel or its alloys. In the latter case (i.e., shaft 100 is electrically conductive), probe 20 includes an electrically insulating jacket 108, which is typically formed as one or more electrically insulating sheaths or coatings, such as polytetrafluoroethylene, polyimide, and the like. The provision of electrically insulating jacket 108 over shaft 100 prevents direct electrical contact between the metal shaft and any adjacent body structure or the surgeon. Such direct electrical contact between a body structure (e.g., heart, bone, nerves, skin, or other blood vessels) and an exposed electrode could result in unwanted heating and necrosis of the structure at the point of contact.

Handle 204 typically comprises a plastic material that is easily molded into a suitable shape for handling by the surgeon. Handle 204 defines an inner cavity (not shown) that houses an electrical connections unit 250 (Fig. 5), and provides a suitable interface for coupling probe 20 to power supply 28 via an electrical connecting cable. Electrode support member 102 extends from the distal end of shaft 100 (usually about 1 mm to 20 mm), and provides support for an active electrode or a plurality of electrically isolated active electrodes 104. In the specific configuration shown in Fig. 2, probe 20 includes a plurality of active electrodes. As shown in Fig. 2, a fluid tube 233 extends through an opening in handle 204, and includes a connector 235 for connection to a fluid supply source for supplying electrically conductive fluid to the target site. Fluid tube 233 is coupled to a distal fluid tube 239 that extends along the outer surface of shaft 100 to an opening 237 at the distal end of the probe 20, as will be discussed in detail below. Of course, the invention is not limited to this configuration. For example, fluid tube 233 may extend through a single lumen (not shown) in shaft 100, it may be coupled to a plurality of lumina (also not shown) that extend through shaft 100 to a plurality of openings at its distal end, or the fluid tube may be completely independent of shaft

100. Probe 20 may also include a valve or equivalent structure for controlling the flow rate of the electrically conductive fluid to the target site.

As shown in Figs. 3 and 4, electrode support member 102 has a substantially planar tissue treatment surface 212 and comprises a suitable insulating material (*e.g.*, a ceramic or glass material, such as alumina, zirconia, and the like) which could be formed at the time of manufacture in a flat, hemispherical or other shape according to the requirements of a particular procedure. The preferred support member material is alumina (Kyocera Industrial Ceramics Corporation, Elk Grove, Illinois), because of its high thermal conductivity, good electrically insulative properties, high flexural modulus, resistance to carbon tracking, biocompatibility, and high melting point. Electrode support member 102 is adhesively joined to a tubular support member (not shown) that extends most or all of the distance between support member 102 and the proximal end of probe 20. The tubular member preferably comprises an electrically insulating material, such as an epoxy or silicone-based material.

In a preferred construction technique, active electrodes 104 extend through pre-formed openings in the support member 102 so that they protrude above tissue treatment surface 212 by the desired distance. The electrodes are then bonded to the tissue treatment surface 212 of support member 102, typically by an inorganic sealing material. The sealing material is selected to provide effective electrical insulation, and good adhesion to both support member 102 and active electrodes 104. In one embodiment, active electrodes 104 comprise an electrically conducting, corrosion resistant metal, such as platinum or titanium. The sealing material additionally should have a compatible thermal expansion coefficient and a melting point well below that of platinum or titanium and alumina or zirconia, typically being a glass or glass ceramic.

In the embodiment shown in Figs. 2-5, probe 20 includes a return electrode 112 for completing the current path between active electrodes 104 and a high frequency power supply 28 (see Fig. 1). As shown, return electrode 112 preferably comprises an annular conductive band coupled to the distal end of shaft 100 at a location proximal to tissue treatment surface 212 of electrode support member 102, typically about 0.5 mm to 10 mm proximal to surface 212, and more

preferably about 1 mm to 10 mm proximal to surface 212. Return electrode 112 is coupled to a connector 258 that extends to the proximal end of probe 20, where it is suitably connected to power supply 28 (Figs. 1 and 2).

As shown in Fig. 2, return electrode 112 is not directly connected to active electrodes 104. To complete this current path so that active electrodes 104 are electrically connected to return electrode 112, electrically conductive fluid (e.g., isotonic saline) is caused to flow therebetween. In the representative embodiment, the electrically conductive fluid is delivered through an external fluid tube 239 to opening 237, as described above (Figs. 2 and 4). Alternatively, the fluid may be continuously delivered by a fluid delivery element (not shown) that is separate from probe 20.

In alternative embodiments, the fluid path may be formed in probe 20 by, for example, an inner lumen or an annular gap between the return electrode and a tubular support member within shaft 100 (not shown). This annular gap may be formed near the perimeter of the shaft 100 such that the electrically conductive fluid tends to flow radially inward towards the target site, or it may be formed towards the center of shaft 100 so that the fluid flows radially outward. In both of these embodiments, a fluid source (e.g., a bag of fluid elevated above the surgical site or having a pumping device), is coupled to probe 20 via a fluid supply tube (not shown) that may or may not have a controllable valve. A more complete description of an electrosurgical probe incorporating one or more fluid lumen(s) can be found in U.S. Patent No. 5,697,281, filed on June 7, 1995, the complete disclosure of which is incorporated herein by reference.

Referring to Figs. 3 and 4, the electrically isolated active electrodes 104 are preferably spaced from each other and aligned to form a linear array 105 of electrodes for cutting a substantially linear incision in the tissue. The tissue treatment surface and individual active electrodes 104 will usually have dimensions within the ranges set forth above. Active electrodes 104 preferably have a distal edge 107 to increase the electric field intensities around terminals 104, and to facilitate cutting of tissue. Thus, active electrodes 104 have a screwdriver shape in the representative embodiment of Figs. 2-4. In one representative embodiment, the tissue treatment surface 212 has a circular cross-sectional shape with a diameter in

the range of about 1 mm to 30 mm, usually about 2 mm to 20 mm. The individual active electrodes 104 preferably extend outward from tissue treatment surface 212 by a distance of about 0.1 mm to 8 mm, usually about 1 mm to 4 mm. Applicant has found that this configuration increases the high electric field intensities and associated current densities around active electrodes 104 to facilitate the ablation of tissue as described in detail above.

Probe 20 may include a suction or aspiration lumen 213 (see Fig. 2) within shaft 100 and a suction tube 211 (Fig. 2) for aspirating tissue, fluids and/or gases from the target site. In this embodiment, the electrically conductive fluid generally flows from opening 237 of fluid tube 239 radially inward and then back through one or more openings (not shown) in support member 102. Aspirating the electrically conductive fluid during surgery allows the surgeon to see the target site, and it prevents the fluid from flowing into the patient's body (e.g., the thoracic cavity). This aspiration should be controlled, however, so that the conductive fluid maintains a conductive path between the active electrode(s) and the return electrode. In some embodiments, the probe 20 will also include one or more aspiration electrode(s) (not shown) coupled to the aspiration lumen for inhibiting clogging during aspiration of tissue fragments from the surgical site. A more complete description of these embodiments can be found in commonly assigned co-pending U.S. Patent Application Serial No. 09/010,382, filed January 21, 1998, the complete disclosure of which is incorporated herein by reference for all purposes.

Fig. 5 illustrates the electrical connections 250 within handle 204 for coupling active electrodes 104 and return electrode 112 to the power supply 28. As shown, a plurality of wires 252 extend through shaft 100 to couple electrodes 104 to a plurality of pins 254, which are plugged into a connector block 256 for coupling to a connecting cable 22 (Fig. 1). Similarly, return electrode 112 is coupled to connector block 256 via a wire 258 and a plug 260.

According to the present invention, probe 20 further includes an identification element that is characteristic of the particular electrode assembly so that the same power supply 28 can be used for different electrosurgical operations. In one embodiment, for example, probe 20 includes a voltage reduction element or a voltage reduction circuit for reducing the voltage applied between the active

electrodes 104 and the return electrode 112. The voltage reduction element serves to reduce the voltage applied by the power supply so that the voltage between the active electrodes and the return electrode is low enough to avoid excessive power dissipation into the electrically conductive medium and/or the tissue at the target site. The voltage reduction element primarily allows the electrosurgical probe 10/20 to be compatible with a range of different power supplies that are adapted to apply higher voltages for ablation or vaporization of tissue (e.g., various power supplies or generators manufactured by ArthroCare Corporation, Sunnyvale, CA). For contraction of tissue, for example, the voltage reduction element will serve to reduce a voltage of about 100 to 135 volts RMS (which corresponds to a setting of 1 on the ArthroCare Model 970 and 980 (i.e., 2000) Generators) to about 45 to 60 volts RMS, which is a suitable voltage for contraction of tissue without ablation (e.g., molecular dissociation) of the tissue.

Again with reference to Fig. 5, in the representative embodiment the voltage reduction element is a dropping capacitor 262 which has a first leg 264 coupled to the return electrode wire 258 and a second leg 266 coupled to connector block 256. Of course, the capacitor may be located in other places within the system, such as in, or distributed along the length of, the cable, the power supply, the connector, etc. In addition, it will be recognized that other voltage reduction elements, such as diodes, transistors, inductors, resistors, capacitors or combinations thereof, may be used in conjunction with the present invention. For example, probe 20 may include a coded resistor (not shown) that is constructed to lower the voltage applied between return electrode 112 and active electrodes 104 to a suitable level for contraction of tissue. In addition, electrical circuits may be employed for this purpose.

Alternatively or additionally, the cable 22 that couples the power supply 28 to probe 10/20 may be used as a voltage reduction element. The cable has an inherent capacitance that can be used to reduce the power supply voltage if the cable is placed into the electrical circuit between the power supply, the active electrodes and the return electrode. In this embodiment, the cable 22 may be used alone, or in combination with one of the voltage reduction elements discussed above, e.g., a capacitor.

Further, it should be noted that various electrosurgical probes of the present invention can be used with a particular power supply that is adapted to apply a voltage within a selected range for a certain procedure or treatment. In which case, a voltage reduction element or circuitry may not be necessary nor desired.

5 With reference to Figs. 6-8, electrode support member 70 according to one embodiment includes a multi-layer substrate comprising a suitable high temperature, electrically insulating material, such as ceramic. The multi-layer substrate is a thin or thick-film hybrid having conductive strips that are adhered to the ceramic wafer layers (e.g., thick-film printed and fired onto or plated onto the
10 ceramic wafers). The conductive strips typically comprise tungsten, gold, nickel, silver, platinum or equivalent materials. In the exemplary embodiment, the conductive strips comprise tungsten, and they are co-fired together with the wafer layers to form an integral package. The conductive strips are coupled to external wire connectors by holes or vias that are drilled through the ceramic layers, and
15 plated or otherwise covered with conductive material. A more complete description of such support members 370 can be found in U.S. Patent Application No. 08/977,845, filed November 25, 1997 (Attorney Docket No. D-2), the entire disclosure of which is incorporated herein by reference.

 In the representative embodiment, support member 70 comprises five
20 ceramic layers 200, 202, 204, 206, 208 (see Figs. 6-10), three gold plated active electrodes 210a, 210b, 210c and first and second gold plated return electrodes 216, 218. As shown in Figs. 9A and 9B, a first ceramic layer 200, which is one of the outer layers of support 70, includes first gold plated return electrode 216 on a lateral surface 220 of layer 200. First ceramic layer 200 further includes a gold conductive
25 strip 222 extending from return electrode 216 to the proximal end of layer 200 for coupling to a lead wire (not shown), and three gold conductive lines 224, 226, 228 extending from a mid-portion of layer 200 to its proximal end. Conductive strips 224, 226, 228 are each coupled to one of the active electrodes 210a, 210b, 210c by conductive holes or vias 230, 232, 234, respectively. As shown, all three vias 230,
30 232, 234 extend through wafer layer 200.

Referring to Figs. 10A and 10B, a second wafer layer 202 is bonded between first outer wafer layer 200 and a middle wafer layer 204 (See Figs. 11A

and 11B). As shown, first active electrode 210a is attached to the distal surface of second wafer layer 202, and a conductive strip 240 extends to via 230 to couple active electrode 210a to a lead wire. Similarly, wafer layers 204 and 206 (Figs. 11A, 11B, 12A, and 12B) each have an active electrode 210b, 210c plated to their distal surfaces, and a conductive strip 242, 244, respectively, extending to one of the vias 232, 234, respectively. Note that the vias only extend as far as necessary through the ceramic layers. As shown in Fig. 13, a second outer wafer layer 208 has a second return electrode 218 plated to the lateral surface 250 of layer 208. The second return electrode 218 is coupled directly to the first return electrode 216 through a via 252 extending through the entire ceramic substrate.

Of course, it will be recognized that a variety of different types of single layer and multi-layer wafers may be constructed according to the present invention. For example, Figs. 14 and 15 illustrate an alternative embodiment of the multi-layer ceramic wafer, wherein the active electrodes comprise planar strips 280 that are plated or otherwise bonded between the ceramic wafer layers 282. Each of the planar strips 280 has a different length, as shown in Fig. 15, so that the active electrodes can be electrically isolated from each other, and coupled to lead wires by vias (not shown).

Fig. 16 illustrates an electrosurgical probe 20' according to another embodiment of the present invention. Probe 20' generally includes handle 104 attached to shaft 100, and has a single, thin, elongated active blade electrode 58. Active electrode 58 is mechanically and electrically separated from return electrode 112 by a support structure 102. The active blade electrode 58 has a sharp distal edge 59 which helps facilitate the cutting process, and sides 62 which contact the tissue (e.g., bone) as the blade electrode 58 passes through the tissue or body structure. By contacting the sides of the blade electrode 58 directly with the tissue or body structure, the electrical power supplied to electrode 58 by power supply 28 can provide hemostasis to the body structure during the cutting process. Optionally, probe 20' can further include one or more coagulation electrode(s) (not shown) configured to seal a severed vessel, bone, or other tissue that is being incised. Such coagulation electrode(s) may be configured such that a single voltage can be applied to coagulate with the coagulation electrode(s) while ablating tissue with the active

electrode(s). According to one aspect of the invention, probe 20' is particularly useful for creating an incision in a patient's chest. For example, in an open-chest CABG procedure a median sternotomy is first performed in which the sternum is sectioned longitudinally so as to allow the chest to be opened for access to the thoracic cavity. Active electrodes 58 include distal edge 59 suitable for sectioning the sternum, and sides 62 suitable for arresting bone bleeding within the incised sternum. Sides 62 are configured to slidably engage the sternum as active electrode 58 is moved with respect to the sternum. Return electrode 112 is spaced proximally from active electrode 58 such that the electrical current is drawn away from the surrounding tissue. Alternatively, the return electrode 112 may be a dispersive pad located on the external surface of the patient's body. By minimizing bleeding of the sternum during an open-chest procedure, the patient's recovery time can be substantially shortened and patient suffering is alleviated.

Figs. 17A-17C schematically illustrate the distal portion of three different embodiments of a probe 90 according to the present invention. As shown in Fig. 17A, active electrodes 104 are anchored in a support 102 of suitable insulating material (*e.g.*, ceramic or glass material, such as alumina, zirconia and the like) which could be formed at the time of manufacture in a flat, hemispherical or other shape according to the requirements of a particular procedure. In one embodiment, the support material is alumina, available from Kyocera Industrial Ceramics Corporation, Elk Grove, Illinois, because of its high thermal conductivity, good electrically insulative properties, high flexural modulus, resistance to carbon tracking, biocompatibility, and high melting point. The support 102 is adhesively joined to a tubular support member 78 that extends most or all of the distance between matrix 102 and the proximal end of probe 90. Tubular member 78 preferably comprises an electrically insulating material, such as an epoxy or silicone-based material.

According to one construction technique, active electrodes 104 extend through pre-formed openings in the support 102 so that they protrude above tissue treatment surface 212 by the desired distance. The electrodes are then bonded to the tissue treatment surface 212 of support 102, typically by an inorganic sealing material 80. Sealing material 80 is selected to provide effective electrical insulation,

and good adhesion to both the support 102 and the platinum or titanium active electrodes. Sealing material 80 additionally should have a compatible thermal expansion coefficient, and a melting point well below that of platinum or titanium and alumina or zirconia, typically being a glass or glass ceramic.

5 In the embodiment shown in Fig. 17A, return electrode 112 comprises an annular member positioned around the exterior of shaft 100 of probe 90. Return electrode 112 may fully or partially circumscribe tubular member 78 to form an annular gap 54 therebetween for flow of electrically conductive liquid 50 therethrough, as discussed below. Gap 54 preferably has a width in the range of
10 0.25 mm to 4 mm. Alternatively, probe 90 may include a plurality of longitudinal ribs between tubular member 78 and return electrode 112 to form a plurality of fluid lumina extending along the perimeter of shaft 100. In this embodiment, the plurality of lumina will extend to a plurality of openings.

Return electrode 112 is disposed within an electrically insulative
15 jacket 17, which is typically formed as one or more electrically insulative sheaths or coatings, such as polytetrafluoroethylene, polyimide, and the like. The provision of the electrically insulative jacket 17 over return electrode 112 prevents direct electrical contact between return electrode 112 and any adjacent body structure. Such direct electrical contact between a body structure (*e.g.*, the heart) and an
20 exposed electrode member 112 could result in unwanted heating and necrosis of the structure at the point of contact.

As shown in Fig. 17A, return electrode 112 is not directly connected to active electrodes 104. To complete a current path so that active electrodes 104 are electrically connected to return electrode 112, electrically conductive liquid 50
25 (*e.g.*, isotonic saline) is caused to flow along fluid path(s) 83. Fluid path 83 is formed by annular gap 54 between outer return electrode 112 and tubular support member 78. The electrically conductive liquid 50 flowing through fluid path 83 provides a pathway for electrical current flow between active electrodes 104 and return electrode 112, as illustrated by the current flux lines 60 in Fig. 17A. When a
30 voltage difference is applied between active electrodes 104 and return electrode 112, high electric field intensities will be generated at the distal tips of active electrodes

104 with current flow from electrodes 104 through the target tissue to the return electrode, the high electric field intensities causing ablation of tissue 52 in zone 88.

Fig. 17B illustrates another alternative embodiment of electrosurgical probe 90 which has a return electrode 112 positioned within tubular member 78.

5 Return electrode 112 may comprise a tubular member defining an inner lumen 57 for allowing electrically conductive liquid 50 (e.g., isotonic saline) to flow therethrough in electrical contact with return electrode 112. In this embodiment, a voltage difference is applied between active electrodes 104 and return electrode 112 resulting in electrical current flow through the electrically conductive liquid 50 as
10 shown by current flux lines 60. As a result of the applied voltage difference and concomitant high electric field intensities at the tips of active electrodes 104, tissue 52 becomes ablated or transected in zone 88.

Fig. 17C illustrates another embodiment of probe 90 that is a combination of the embodiments in Figs. 17A and 17B. As shown, this probe
15 includes both an inner lumen 57 and an outer gap or plurality of outer lumina 54 for flow of electrically conductive fluid. In this embodiment, the return electrode 112 may be positioned within tubular member 78 as in Fig. 17B, outside of tubular member 78 as in Fig. 17A, or in both locations.

Fig. 18 illustrates another embodiment of probe 90 where the distal
20 portion of shaft 100 is bent so that active electrodes extend transversely to the shaft. Preferably, the distal portion of shaft 100 is perpendicular to the rest of the shaft so that tissue treatment surface 212 is generally parallel to the shaft axis. In this embodiment, return electrode 112 is mounted to the outer surface of shaft 100 and is covered with an electrically insulating jacket 17. The electrically conductive fluid
25 50 flows along flow path 83 through return electrode 112 and exits the distal end of electrode 112 at a point proximal of tissue treatment surface 212. The fluid is directed exterior of shaft to surface 212 to create a return current path from active electrodes 104, through the fluid 50, to return electrode 112, as shown by current flux lines 60.

30 Fig. 19 illustrates another embodiment of the invention where electrosurgical system 11 further includes a liquid supply instrument 64 for supplying electrically conductive fluid 50 between active electrodes 104 and a return

electrode 112'. Liquid supply instrument 64 comprises an inner tubular member or return electrode 112' surrounded by an electrically insulating jacket 17. Return electrode 112' defines an inner passage 83 for flow of fluid 50. As shown in Fig. 19, the distal portion of instrument 64 is preferably bent so that liquid 50 is discharged at an angle with respect to instrument 64. This allows the surgical team to position liquid supply instrument 64 adjacent tissue treatment surface 212 with the proximal portion of supply instrument 64 oriented at a similar angle to probe 90.

The present invention is not limited to an electrode array disposed on a relatively planar surface at the distal tip of probe 90, as described above.

Referring to Figs. 20A and 20B, an alternative probe 90 includes a pair of electrodes 105a, 105b mounted to the distal end of shaft 100. Electrodes 105a, 105b are electrically connected to a power supply, as described above, and preferably have tips 107a, 107b having a screwdriver shape. The screwdriver shape provides a greater amount of "edges" to electrodes 105a, 105b, to increase the electric field intensity and current density at tips 107a, 107b, thereby improving the cutting ability as well as the ability to provide hemostasis of the incised tissue.

Fig. 21 illustrates yet another embodiment designed for cutting of body tissue, organs, or structures. In this embodiment, the active electrodes 104 are arranged in a linear or columnar array of one or more closely spaced columns so that as the electrodes 104 are moved along the longer axis (denoted by arrow 160 in Fig. 21), the current flux lines are narrowly confined at the tip of the active electrodes 104 and result in a cutting effect in the body structure being treated. As before, the current flux lines 60 emanating from the active electrodes 104 pass through the electrically conductive liquid to the return electrode structure 112 located proximal to the probe tip.

Referring now to Figs. 22 and 23, alternative geometries are shown for the active electrodes 104. These alternative electrode geometries allow the electrical current densities emanating from the active electrodes 104 to be concentrated to achieve an increased ablation rate and/or a more concentrated ablation effect due to the fact that sharper edges (*i.e.*, regions of smaller radii of curvature) result in higher current densities. Fig. 22 illustrates a flattened extension of a round wire active electrode 104 which results in higher current densities at the

edges 180. Another example is shown in Fig. 23 in which the active electrode 104 is formed into a cone shaped point 182 resulting in higher current densities at the tip of the cone.

Another embodiment of the electrosurgical probe is illustrated in Fig.

5 24. The electrosurgical probe 90 comprises a shaft 100 and at least two active electrodes 104 extending from a support 102 at the distal end of the shaft. The active electrodes 104 preferably define a distal edge 600 for making an incision in tissue. The edges 600 of the active electrodes 104 are substantially parallel with each other and usually spaced a distance of about 4 mm to 15 mm apart, preferably
10 about 8 mm to 10 mm apart. The edges 600 extend from the distal end of support 102 by a distance of about 0.5 mm to 10 mm, preferably about 2 mm to 5 mm. In the exemplary embodiment, probe 90 will include a return electrode 112 spaced proximally from the active electrodes 104. In an alternative embodiment (not shown), one of the active electrodes 104 may function as a return electrode, or the
15 return electrode may be a dispersive pad located on an external surface of the patient's body.

Fig. 25 illustrates a distal portion of an electrosurgical probe 500 according to another embodiment of the present invention. The embodiment of Fig. 25 is particularly useful for cutting or creating incisions in tissue structures. Probe
20 500 comprises a support member 502 coupled to a shaft or disposable tip (not shown) as described in previous embodiments. Support member 502 preferably comprises an inorganic electrically insulating material, such as ceramic, glass, or glass-ceramic. In this embodiment, however, support member 502 may comprise an organic material, such as plastic, because the active electrode 506 and return
25 electrode 508 are both spaced away from support member 502. Thus, the high intensity electric fields may be far enough away from support member 502 so as to allow an organic material.

An electrode assembly 504 extends from a distal end of support member 502, preferably by a distance of about 2 mm to 20 mm. Electrode
30 assembly 504 comprises a single, active electrode 506 and a return electrode sleeve 508 spaced proximally from active electrode 506 by an insulation member 510, which preferably comprises an inorganic material, such as ceramic, glass or glass-

ceramic. As shown, active electrode 506 preferably tapers to a sharp distal end 512 to facilitate the cutting or incising of tissue. In the exemplary embodiment, active electrode 506 has a proximal diameter of about 0.2 to 20 mm and a distal diameter of less than about 0.2 mm. Return electrode 508 is spaced from active electrode 506 a sufficient distance to prevent shorting or arcing therebetween at sufficient voltages to allow the volumetric removal of tissue. In the representative embodiment, the distal exposed portion of return electrode 508 is spaced about 0.5 to about 5 mm from the proximal exposed portion of active electrode 506. Of course, it will be recognized that the present invention is not limited to the particular dimensions and configuration of the electrode assembly 504 described herein, and a variety of different configurations may be envisioned depending on the surgical application.

As shown, probe 500 includes a fluid lumen 520 passing through support member 502 to a distal opening (not shown) at the distal end of support member 502. Fluid lumen 520 is coupled to a supply of electrically conductive fluid, such as isotonic saline, or other suitable conductive fluid for delivery of such fluid to the target site. In the exemplary embodiment, probe 500 is designed such that lumen 520 will be positioned above electrode assembly 504 during use such that the conductive fluid exiting the distal opening of lumen 520 will naturally pass over return electrode 508 and active electrode 506 thereby creating a current path therebetween. In addition, the conductive fluid will be sufficient to cover the active electrode 506 such that the conditions for plasma formation can be met, as described in detail above.

Figs. 26, and 27A-C illustrate another exemplary electrosurgical probe 310 for cutting, incising, or removing tissue structures. Probe 310 comprises a shaft or disposable tip 313 removably coupled to a proximal handle 312, and an electrically insulating electrode support member 370 extending from tip 313 for supporting a plurality of active electrodes 358. Tip 313 and handle 312 typically comprise a plastic material that is easily molded into a suitable shape for handling by the surgeon. As shown in Figs. 27A and 27B, handle 312 defines an inner cavity 372 that houses the electrical connections 374, and provides a suitable interface for connection to electrical connecting cable 34 (see Fig. 1). In the exemplary

embodiment, handle 312 is constructed of a steam autoclavable plastic or metal (e.g., polyethylether ketone, or a stable metal alloy containing aluminum and/or zinc) so that it can be re-used by sterilizing handle 312 between surgical procedures. High service temperature materials are preferred, such as a silicone cable jacket and a poly-ether-imide handpiece or ULTEM® that can withstand repeated exposure to high temperatures.

Referring to Figs. 27A-27C, tip 313 preferably comprises first and second housing halves 500, 502 that snap fit together, and form a recess 404 therebetween for holding electrode support member 370 within the tip 313.

Electrode support member 370 extends from the distal end of tip 313, usually by about 0.5 mm to 20 mm, and provides support for a plurality of electrically isolated active electrodes 358 and one or more return electrodes 400. Alternatively, electrode support member 370 may be recessed from the distal end of tip 313 to help confine the electrically conductive fluid around the active electrodes 358 during the surgical procedure, as discussed above. Electrode support member 370 has a substantially planar tissue treatment surface 380 that is usually disposed at an angle of about 10 to 90 degrees relative to the longitudinal axis of handle 312 to facilitate handling by the surgeon. In the exemplary embodiment, this function is accomplished by orienting tip 313 at an acute angle relative to the longitudinal axis of handle 312.

In the embodiment shown in Figs. 26-27C, probe 310 includes a single annular return electrode 400 for completing the current path between active electrodes 358 and power supply 28 (see Fig. 1). As shown, return electrode 400 preferably has a fluid contact surface slightly proximal to tissue treatment surface 380, typically by about 0.1 mm to 2 mm, and preferably by about 0.2 mm to 1 mm. Return electrode 400 is coupled to a connector 404 that extends to the proximal end of handle 313, where it is suitably connected to power supply 28 (Fig. 1).

Referring again to Figs. 27A-27C, tip 313 further includes a proximal hub 506 for supporting a male electrical connector 508 that holds a plurality of wires 510 each coupled to one of the active electrodes 358 or to return electrode 400 on support member 370. A female connector 520 housed within handle 312 is removably coupled to male connector 508, and a plurality of wires

522 extend from female connector 520 through a strain relief 524 to cable 334. Both sets of wires 510, 522 are insulated to prevent shorting in the event of fluid ingress into the probe 310. This design allows for removable connection of the electrodes in tip 313 with the connector 520 within handle 312 so that the handle can be re-used with different tips 313. Probe 310 will preferably also include an identification element, such as a coded resistor (not shown), for programming a particular voltage output range and mode of operation for the power supply. This allows the power supply to be employed with a variety of different probes for a variety of different applications.

In the representative embodiment, probe 310 includes a fluid tube 410 (Fig. 26) for delivering electrically conductive fluid to the target site. Fluid tube 410 is sized to extend through a groove 414 in handle 313 and through an inner cavity 412 in tip 312 to a distal opening 414 (Fig. 26) located adjacent electrode support member 370. Tube 410 extends all the way through inner cavity 412 to opening 414 to eliminate any possible fluid ingress into cavity 412. Fluid tube 410 includes a proximal connector for coupling to an electrically conductive fluid source 321.

Probe 310 will also include a valve or equivalent structure for controlling the flow rate of the electrically conductive fluid to the target site. In the representative embodiment shown in Figs. 27A-27C, handle 312 comprises a main body 422 coupled between distal hub 418 and strain relief 420, and a rotatable sleeve 416 around main body 422. Distal hub 418 has an opening 419 for receiving proximal hub 506 of tip 313 for removably coupling the tip 313 to the handle 312. Sleeve 416 is rotatably coupled to strain relief 420 and distal hub 418 to provide a valve structure for fluid tube 410. As shown in Fig. 27A, fluid tube 410 extends through groove 414 from strain relief 420, through main body 422 and distal hub 420 to tip 313. Rotation of sleeve 416 will impede, and eventually obstruct, the flow of fluid through tube 410. Of course, this fluid control may be provided by a variety of other input and valve devices, such as switches, buttons, etc.

In alternative embodiments, the fluid path may be directly formed in probe 310 by, for example, a central inner lumen or an annular gap (not shown) within the handle and the tip. This inner lumen may be formed near the perimeter

of the probe 310 such that the electrically conductive fluid tends to flow radially inward towards the target site, or it may be formed towards the center of probe 310 so that the fluid flows radially outward. In addition, the electrically conductive fluid may be delivered from a fluid delivery element (not shown) that is separate from probe 310. In arthroscopic surgery, for example, the body cavity will be flooded with isotonic saline and the probe 310 will be introduced into this flooded cavity. Electrically conductive fluid will be continually resupplied to maintain the conduction path between return electrode 400 and active electrodes 358. A more complete description of alternative electrosurgical probes incorporating one or more fluid lumen(s) can be found in commonly assigned, co-pending Application No. 08/485,219, filed on June 7, 1995 (Attorney Docket 16238-000600), the complete disclosure of which is incorporated herein by reference.

Referring now to Fig. 26, electrically isolated active electrodes 358 are spaced apart over tissue treatment surface 380 of electrode support member 370, preferably in a linear array. In the representative embodiment, three active electrodes 358, each having a substantially conical shape, are arranged in a linear array extending distally from surface 380. Active electrodes 358 will usually extend a distance of about 0.5 mm to 20 mm from tissue treatment surface 380, preferably about 1 mm to 5 mm. Applicant has found that this configuration increases the electric field intensities and associated current densities at the distal edges of active electrodes 358, which increases the rate of tissue cutting. In the representative embodiment, the tissue treatment surface 380 has a circular cross-sectional shape with a diameter in the range of about 0.5 mm to 20 mm (preferably about 2 mm to 10 mm). The individual active electrodes 358 preferably taper outward as shown, or they may form a distal edge, such as the electrodes shown in Figs. 3 and 24.

Probe 430 of Fig. 28 includes a shaft 432 coupled to a proximal handle 434 for holding and controlling shaft 432. Probe 430 includes an active electrode array 436 at the distal tip of shaft 432, an annular return electrode 438 extending through shaft 432 and proximally recessed from the active electrode array 436, and an annular lumen 442 between return electrode 438 and an outer insulating sheath 446. Probe 430 further includes a liquid supply conduit 444 attached to handle 434 and in fluid communication with lumen 442, and a source of electrically

conductive fluid (not shown) for delivering the fluid past return electrode 438 to the target site on the tissue 440. Electrode array 436 is preferably flush with the distal end of shaft 432 or distally extended from the distal end by a small distance (on the order of 0.005 inches) so as to minimize the depth of ablation. Preferably, the distal end of shaft 432 is beveled to improve access and control of probe 430 while treating the target tissue.

Yet another embodiment of the present invention is shown in Fig. 29. Auxiliary active electrodes 458, 459 are positioned at the distal tip 70 of the probe. Auxiliary active electrodes 458, 459 may be the same size as ablation active electrodes 58, or larger as shown in Fig. 29. One operating arrangement is to connect auxiliary active electrodes 458, 459 to two poles of a high frequency power supply to form a bipolar circuit allowing current to flow between the terminals of auxiliary active electrodes 458, 459 as shown by current flux lines 460. Auxiliary active electrodes 458, 459 are electrically isolated from ablation electrodes 58. By proper selection of the inter-electrode spacing, W_2 , and electrode width, W_3 , and the frequency of the applied voltage, the current flux lines 460 can be caused to flow below the target layer as described above.

The voltage will preferably be sufficient to establish high electric field intensities between the active electrode array 436 and the target tissue 440 to thereby induce molecular breakdown or disintegration of several cell layers of the target tissue. As described above, a sufficient voltage will be applied to develop a thin layer of vapor within the electrically conductive fluid and to ionize the vaporized layer or region between the active electrode(s) and the target tissue. Energy in the form of charged particles are discharged from the vapor layer to ablate the target tissue, thereby minimizing necrosis of surrounding tissue and underlying cell layers.

With reference to Fig. 30, there is shown in perspective view an electrosurgical probe 700, according to another embodiment of the invention. Probe 700 includes a shaft 702 having a shaft distal end portion 702a and a shaft proximal end portion 702b. Shaft 702 is affixed at its proximal end 702b to a handle 704. Shaft 702 typically comprises an electrically conductive material, usually a metal, such as tungsten, stainless steel, platinum or its alloys, titanium or its alloys,

molybdenum or its alloys, nickel or its alloys. An electrically insulating electrode support 710 is disposed at shaft distal end 702a. An active electrode 712 is disposed on electrode support 710. Active electrode 712 comprises a blade electrode (e.g., Figs. 31A, 31B). An electrically insulating sleeve 716 covers a portion of shaft 702, and terminates at sleeve distal end 716a to define an exposed portion of shaft 702 extending between electrode support proximal end 710b and sleeve distal end 716a. This exposed portion of shaft 702 defines a return electrode 718 on shaft distal end portion 702a. (In an alternative embodiment, the return electrode may take the form of an annular band of an electrically conductive material, e.g., a platinum alloy, disposed on the exterior of the shaft distal end.) A cavity within handle 704 accommodates a connection block 706 which is connected to active electrode 712 and return electrode 718 via electrode leads (not shown). Connection block 706 provides a convenient mechanism for coupling active electrode 712 and return electrode 718 to opposite poles of a power supply (e.g., power supply 28, Fig. 1).

Fig. 31A is a perspective view of an active electrode 712 of probe 700, according to one embodiment of the invention. Active electrode 712 is in the form of a single blade electrode which extends from electrode support 710 to a distance, H_b . The distance H_b may vary, for example, according to the intended applications of probe 700, and the value of H_b is at least to some extent a matter of design choice. Typically, for a broad array of electrosurgical procedures, the distance H_b is in the range of from about 0.02 mm to about 5 mm. Active electrode 712 includes an active edge 713 which is adapted for generating high current densities thereat upon application of a high frequency voltage from the power supply between active electrode 712 and return electrode 718. In this way, active edge 713 can efficiently effect localized ablation of tissues via molecular dissociation of tissue components which contact, or are in close proximity to, active edge 713. A process for ablation of tissues via molecular dissociation of tissue components has been described hereinabove.

As best seen in Fig. 31B, the blade-like active electrode 712 further includes first and second blade sides, 714a, 714b, respectively. First and second blade sides 714a, 714b are separated by a maximum distance, W_b . The distance W_b is typically in the range of from about 0.1 mm to about 2.5 mm. In the embodiment of Fig. 31B, first and second blade sides 714a, 714b are substantially parallel to each other. Each of first and second blade sides 714a, 714b are adapted for engaging tissue severed, ablated, or otherwise modified by active edge 713, and for coagulating tissue engaged by first blade side 714a and/or second blade side 714b. In this way, active electrode 712 can precisely and effectively sever, ablate, or otherwise modify a target tissue with active edge 713 to form a first-modified tissue, and at the same time, or shortly thereafter, further modify the first-modified tissue by means of first and second blade sides 714a, 714b. For example, active edge 713 can make an incision in a target tissue via localized molecular dissociation of target tissue components, while first and second blade sides 714a, 714b can effect hemostasis in the severed tissue.

Figs. 32A, 32B, and 32C are a side view, a plan view, and an end view, respectively, of electrosurgical probe 700 having a blade-like active electrode 712, according to one embodiment of the invention. In the embodiment of Figs. 32A-C, electrode support 710 is disposed at the terminus of shaft 702, and active electrode 712 is affixed to support distal end 710a (e.g., Fig. 33A). However, other arrangements for electrode support 710 and active electrode 712 are within the scope of the invention (e.g., Figs. 34A-C, 35A-C). Active electrode 712 is in the form of a substantially flat metal blade. Active electrode 712 is shown as being substantially rectangular as seen from the side (Fig. 32A). However, various other shapes for active electrode 712 are within the scope of the invention (e.g., Figs. 33C-E). Fig. 32C is an end view of probe 700 as seen along the lines 32C-32C of Fig. 32B, showing a laterally compressed region 703 of shaft 702. Laterally compressed region 703 may be adapted for housing electrode support 710. Laterally compressed region 703 may also facilitate manipulation of shaft distal end portion 702a of probe 700 during various surgical procedures, particularly in situations where accessibility of a target tissue is restricted.

Figs. 33A and 33B are a side view and a plan view, respectively, of the distal end of probe 700, showing details of shaft distal end portion 702a and terminally disposed blade active electrode 712, according to one embodiment of the invention. Blade electrode 712 is substantially rectangular in shape as seen from the side (Fig. 33A). The distal end of shaft 702 includes laterally compressed region 703. As seen from the side (Fig. 33A), laterally compressed region 703 appears wider than more proximal portions of shaft 702. Fig. 33B is a plan view of probe 700 as seen along the lines 33B-33B of Fig. 33A, in which laterally compressed region 703 appears narrower than more proximal portions of shaft 702. Electrode support 710 is mounted to the distal end of laterally compressed region 703. Typically, electrode support 710 comprises a durable, electrically insulating, refractory material having a certain amount of flexibility. For example, electrode support 710 may comprise a material such as a silicone rubber, a polyimide, a fluoropolymer, a ceramic, or a glass.

Figs. 33C-33E each show a side view of the distal end of probe 700 having a terminal blade active electrode 712, according to three different embodiments of the invention. Electrode support 710 is mounted terminally on shaft 702, and includes a support distal end 710a and a support proximal end 710b. In the embodiment of Fig. 33C, active edge 713 of active electrode 712 is arcuate, convex, or substantially semi-circular in shape. In the embodiment of Fig. 33D, active electrode 712 has a pointed active edge 713, while in the embodiment of Fig. 33E, the active edge 713 of active electrode 712 is serrated.

Fig. 34A shows in side view an electrosurgical probe 700 having electrode support 710 mounted terminally on shaft 702 and blade active electrode 712 disposed laterally on electrode support 710, according to another embodiment of the invention. Fig. 34B is a plan view of probe 700 taken along the lines 34B-34B of Fig. 34A. Fig. 34C is an end view taken along the lines 34C-34C of Fig. 34A. In the embodiments of Figs 34A-C, electrode 712 is in the form a substantially flat, metal blade having first and second blade sides 714a, 714b, substantially parallel to each other. First and second blade sides 714a, 714b are adapted for engaging and coagulating severed or modified tissue, as described hereinabove.

Fig. 35A shows in side view an electrosurgical probe 700 having electrode support 710 mounted laterally on the distal end of shaft 702, according to another embodiment of the invention. Blade active electrode 712 is mounted laterally on electrode support 710. Fig. 35B is a plan view of probe 700 taken along the lines 35B-35B of Fig. 35A. Fig. 35C is an end view taken along the lines 35C-35C of Fig. 35A. Active electrode 712 is in the form a substantially flat, metal blade having first and second blade sides 714a, 714b, substantially parallel to each other. Electrode support 710 is mounted laterally on laterally compressed region 703 of shaft 702.

Fig. 36A shows a side view of the distal end of an electrosurgical probe 700, wherein shaft 702 includes a beveled end 728 to which electrode support 710 is mounted. Blade active electrode 712 is disposed on electrode support 710. The arrangement of electrode support 710 and electrode 712 on beveled end 728 may facilitate access of shaft distal end portion 702a in general, and of electrode 712 in particular, to a target tissue during various surgical procedures, particularly in situations where accessibility is restricted. Fig. 36B shows a side view of the distal end of an electrosurgical probe 700, according to another embodiment of the invention. Shaft 702 includes a curved distal end 702a'. Electrode support 710 is mounted on distal end 702a', and blade active electrode 712 is affixed to electrode support 710. Curved distal end 702a' facilitates access of electrode 712 to a target tissue during various surgical procedures.

Although in the embodiments of Figs. 34A-C, 35A-C, and 36A-B active electrode 712 is shown as being substantially rectangular, this representation should not be construed as limiting these embodiments to a rectangular active electrode 712. Indeed, each of the embodiments of Figs. 34A-C, 35A-C, and 36A-B may have an active electrode 712 in a broad range of shapes, including those represented in Figs. 33C-E.

Fig. 37A shows in side view an electrosurgical probe 700 having an exterior tube 724 arranged on shaft 702 and coupled at its proximal end to a connection tube 720 at handle 704. Exterior tube 724 may comprise a plastic tube of suitable length commensurate with the size of probe 700. Exterior tube 724 defines a lumen 726, and typically terminates at shaft distal end 702a at a location somewhat proximal to electrode support 710. In some embodiments, probe 700 may include two or more exterior tubes 724, each exterior tube 724 having lumen 726. Each lumen 726 may serve as a conduit for an aspiration stream, or as a conduit for delivery of an electrically conductive fluid to the shaft distal end, generally as described hereinabove. Fig. 37B is an end view of probe 700 taken along the lines 37B-37B of Fig. 37A, showing exterior tube 724 and lumen 726 in relation to shaft 702. The diameter of exterior tube 724 is, at least to some extent, a matter of design choice. Exterior tube 724 may comprise a substantially rigid or somewhat flexible plastic tube comprising polyethylene, a polyimide, a fluoropolymer, and the like.

Fig. 38A shows, in side view, an electrosurgical probe 700 having an outer sheath 722 surrounding the exterior of a portion of shaft 702, according to another embodiment of the invention. Outer sheath 722 is coupled at its proximal end to a connection tube 720 at handle 704. Outer sheath 722 may comprise a plastic tube of suitable length and having a diameter larger than that of shaft 702. Together with the exterior of shaft 702, outer sheath 722 defines a lumen 726' in the form of an annular void. Typically, outer sheath 722 terminates at shaft distal end 702a at a location proximal to electrode support 710. Lumen 726' typically serves as a conduit for delivery of an electrically conductive fluid to the shaft distal end. Fig. 38B is an end view of probe 700 taken along the lines 38B-38B of Fig. 38A, showing outer sheath 722 and lumen 726' in relation to shaft 702. The diameter of outer sheath 722 is, at least to some extent, a matter of design choice. Outer sheath 722 may comprise a substantially rigid or somewhat flexible plastic tube comprising polyethylene, a polyimide, and the like.

Fig. 39A schematically represents an electrosurgical probe 700, according to another embodiment of the invention. Probe 700 includes shaft 702 and handle 704 affixed at shaft proximal end 702b. A first electrode support 711a

and a second electrode support 711b are disposed at shaft proximal end 702a. A blade active electrode 712 is arranged on first and second electrode supports, 711a, 711b. Each of first and second electrode supports 711a, 711b may comprise a refractory and electrically insulating material, such as a silicone rubber or the like, as described hereinabove. A return electrode 718 is located at shaft distal end 702 proximal to first and second electrode supports 711a, 711b. Return electrode 718 may comprise an exposed portion of shaft distal end 702a (e.g., Figs. 32A-C). Blade active electrode 712 typically extends distally from electrode support 710 by a distance in the range of from about 0.1 mm to about 10 mm, an more typically from about 2 mm to 10 mm.

Blade active electrode 712 and return electrode 718 may be independently coupled to opposite poles of a high frequency power supply via electrode leads (not shown) and a connection block (e.g., Fig. 30). In one embodiment, an active electrode lead is coupled to one of first and second electrode arms 715a, 715b, and the other arm terminates in a free, electrically isolated end, for example, within first electrode support 711a or second electrode support 711b. Blade active electrode 712 includes a crosspiece 715c (Figs. 39B-D) located distal to aspiration port 734. A fluid delivery element or unit including an outer sheath 722' (e.g., Fig. 39B) is omitted from Fig. 39A for the sake of clarity.

Fig. 39B is a partial sectional view of probe 700 of Fig. 39A as seen from the side. Outer sheath 722' defines an annular fluid delivery lumen 726' between sheath 722' and shaft 702. Lumen 726' terminates in an annular fluid delivery port 725 at shaft distal end 702a. Fluid delivery lumen 726' is in communication proximally with a fluid delivery tube 721. Solid arrows indicate the direction of flow of an electrically conductive fluid (e.g., isotonic saline) within fluid delivery lumen 726'. Aspiration port 734 is in communication proximally with an aspiration lumen 732 and an aspiration tube 730. Solid arrows within aspiration lumen 732 indicate the direction of flow of an aspiration stream, which flows from aspiration port 734 towards a source of vacuum (not shown), the latter coupled to aspiration tube 730. Fig. 39C is an end view of probe 700 taken along the lines 39C-39C of Fig. 39B. Active electrode 712 includes crosspiece 715c extending between first and second electrode arms 715a, 715b, respectively (Fig. 39D).

Active electrode 712 further includes first and second blade sides 714a, 714b. In some embodiments, first and second blade sides 714a, 714b are adapted for engaging tissue that has been severed, and for coagulating the severed tissue. Crosspiece 715c at least partially spans aspiration port 734. Typically, active electrode 712 comprises a single metal blade, comprising a material such as platinum, tungsten, palladium, iridium, or titanium, or their alloys.

Fig. 39D shows detail of the distal portion of probe 700 of Figs. 39A-C including blade active electrode 712. As shown, first and second electrode arms 715a, 715b are disposed on first and second electrode supports 711a, 711b, respectively. In an alternative embodiment, first and second electrode arms 715a, 715b may be disposed on a single annular electrode support having a substantially central void defining aspiration port 734. In one embodiment, active electrode 712 includes both a distal active edge 713a, and a proximal active edge 713b. Distal active edge 713a, in particular, is adapted for aggressively ablating tissue via molecular dissociation of tissue components and for severing tissue targeted for resection, transection, dissection, or other treatment.

Fig. 40A is a partial sectional view of an electrosurgical probe 700 according to another embodiment of the invention. Probe 700 of Fig. 40A generally includes shaft 702 and handle 704, together with a fluid delivery element, and an aspiration unit, essentially as for the embodiment described with reference to Figs. 39A-D. In the interests of brevity these elements and features will not be described in detail with reference to Figs. 40A-C. The embodiment of Fig. 40A differs from other embodiments described herein in having an active electrode in the form of a plasma hook 712'. Hook 712' is in some respects analogous to plasma blade electrodes described hereinabove. For example, in one respect hook 712' is analogous to a truncated version of electrode 712 of the embodiment of Figs. 39A-D in which one of arms 715a or 715b is omitted leaving one electrode arm affixed to crosspiece 715c. From a functional standpoint, hook 712' allows the operator (surgeon) to ablate tissue by drawing the instrument towards himself/herself. In this manner, greater control is exerted over the amount or extent of tissue removed or severed by probe 700. Hook 712' includes a first axial portion 712'a (Fig. 40C) in contact at its proximal end with electrode support 710. Hook 712' may further

include a second portion 712'b extending from the distal portion of first axial portion 712'a. In some embodiments, second portion 712'b is arranged substantially orthogonal to first axial portion 712'a. In one embodiment, second portion 712'b may be structurally similar or analogous to crosspiece 715c of the embodiment of Figs. 39A-D. Second portion 712'b at least partially spans aspiration port 734 (Fig. 40B). Electrode support 710 may comprise a refractory and electrically insulating material, such as a silicone rubber or the like, as described hereinabove.

Fig. 40B shows an end view of probe 700 taken along the lines 40B-40B of Fig. 40A. Hook 712' includes first and second blade sides 714a, 714b. Second portion 712'b extends at least partially across aspiration port 734. Fig. 40C shows detail of the distal end portion of probe 700 of Figs. 40A, 40B, including hook 712'. Hook 712' includes a distal active edge 713a, a proximal active edge 713b, and an active tip 713c. Return electrode 718 is located proximal to electrode support 710. Upon application of a high frequency voltage between hook 712' and return electrode 718, a high current density may be generated at each of distal active edge 713a, proximal active edge 713b, and active tip 713c. Each of distal active edge 713a, proximal active edge 713b, and active tip 713c may be adapted for severing tissue via electrosurgical molecular dissociation of tissue components.

Figs. 41A, 41B, and 41C each show detail of the distal end portion of an electrosurgical probe including a hook electrode 712', according to three different embodiments of the invention. In the embodiment of Fig. 41A, hook 712' is curved, having a convex distal edge 713a, and a concave proximal edge 713b. In the embodiment of Fig. 41B, proximal edge 713b includes serrations thereon. In an alternative embodiment (not shown), distal edge 713a, and/or active tip 713c may be similarly serrated. In the embodiment of Fig. 41C, hook 712' is curved, having a concave distal edge 713a, and a convex proximal edge 713b. According to various embodiments of probe 700, second portion 712'b may have a length which is less than, equal to, or greater than the diameter of shaft 702. In the latter case, second portion 712'b extends laterally beyond the exterior surface of shaft 702 (e.g., Fig. 41C). In each of the embodiments of Figs. 41A-C, hook 712' typically comprises a single blade having first and second blade sides 714a, 714b (e.g., Fig. 40B). Hook

712' typically comprises a metal such as platinum, tungsten, palladium, iridium, or titanium, or their alloys.

Figs. 42A-B schematically represent a process during treatment of a patient with electrosurgical probe 700. Blade active electrode 712 is affixed to support 710 on shaft 702. Blade active electrode 712 includes active edge 713 and first and second blade sides, 714a, 714b (e.g., Figs. 31A-B). Referring to Fig. 42A, active edge 713 forms an incision, I, in a target tissue, T, via localized molecular dissociation of tissue components upon application of a high frequency voltage between active electrode 712 and return electrode 718. (The localized molecular dissociation may be facilitated by the delivery of a suitable quantity of an electrically conductive fluid (e.g. isotonic saline) to form a current flow path between active electrode 712 and return electrode 718.) With reference to Fig. 42B, as the incision I is deepened within tissue T, first and second blade sides, 714a, 714b engage severed tissue in regions indicated by the arrows labeled E. In this way, the severed tissue is coagulated by first and second blade sides, 714a, 714b, thereby effecting hemostasis at the point of incision of the tissue.

Fig. 43A schematically represents a number of steps involved in a method of treating a patient with an electrosurgical probe, wherein step 1000 involves positioning the distal end of the probe adjacent to target tissue such that an active electrode of the probe is in contact with or in close proximity to the target tissue. In one embodiment, the active electrode is spaced a short distance from the target tissue, as described hereinabove. Typically, step 1000 involves positioning the probe such that an active edge of the active electrode makes contact with, or is in close proximity to, the target tissue. Step 1002 involves delivering an electrically conductive fluid to the distal end of the probe in the vicinity of the active electrode and the return electrode, such that the electrically conductive fluid forms a current flow path between the active electrode and the return electrode. The electrically conductive fluid may be delivered via an exterior tube disposed on the outside of the shaft (e.g., Figs. 37A, 37B), or an outer sheath external to the shaft and forming an annular fluid delivery lumen (e.g., Figs. 38A, 38B). The electrically conductive fluid may be a liquid, a gel, or a gas. Apart from providing an efficient current flow path between the active and return electrodes, a clear, colorless electrically

conductive liquid, such as isotonic saline, exhibits the added advantage of increasing the visibility of the surgeon at the target site. However, in situations where there is an abundance of electrically conductive body fluids (e.g., blood, synovial fluid) already present at the target site, step 1002 may optionally be omitted.

5 Step 1004 involves applying a high frequency voltage between the active electrode and the return electrode sufficient to ablate or otherwise modify the target tissue via localized molecular dissociation of target tissue components. By delivering an appropriate high frequency voltage to a suitably configured probe, the target tissue can be incised, dissected, transected, contracted, or otherwise modified.

10 In addition, the modified tissue can also be coagulated (e.g., Fig. 42B). The frequency of the applied voltage will generally be within the ranges cited hereinabove. For example, the frequency will typically range from about 5 kHz to 20 MHz, usually from about 30 kHz to 2.5 MHz, and often between about 100 kHz and 200 kHz. The root mean square (RMS) voltage that is applied in step 1004 is

15 generally in the range of from about 5 volts to 1000 volts RMS, more typically being in the range of from about 10 volts to 500 volts RMS. The actual voltage applied may depend on a number of factors, including the size of the active electrode, the operating frequency, and the particular procedure or desired type of modification of the tissue (incision, contraction, etc.), as described hereinabove.

20 Step 1006 involves manipulating the probe with respect to the tissue at the target site. For example, the probe may be manipulated such that an active edge of a blade or hook electrode reciprocates with respect to the target tissue, such that the target tissue is severed, incised, or transected at the point of movement of the active edge by a process involving molecular dissociation of tissue components.

25 In embodiments where the active electrode is in the form of a hook, step 1006 may involve engaging the hook against the target tissue and drawing the hook towards the operator in order to cut or sever the tissue. In this manner, the extent of cutting or severing can be precisely controlled. In one embodiment, step 1006 involves reciprocating an active edge in a direction parallel to a surface of the target tissue.

30 Typically, step 1006 is performed concurrently with step 1004. Step 1002 may be performed at any stage during the procedure, and the rate of delivery of the electrically conductive fluid may be regulated by a suitable mechanism, such as a

valve.

Step 1008 involves modifying the target tissue as a result of the high frequency voltage applied in step 1004. The target tissue may be modified in a variety of different ways, as referred to hereinabove. The type of tissue modification achieved depends, *inter alia*, on the voltage parameters of step 1004; the shape, size, and composition of the active electrode; and the manner in which the probe is manipulated by the surgeon in step 1006. At relatively high voltage levels, tissue components typically undergo localized molecular dissociation, whereby the target tissue can be dissected, incised, transected, etc. At a lower voltage, or at a lower current density on the active electrode surface, the target tissue can be contracted (e.g., by shrinkage of collagen fibers in the tissue), or a blood vessel can be coagulated. For example, in step 1010 the first and second blade sides of the active electrode may be engaged against a region of the target tissue which has been modified as a result of localized molecular dissociation of tissue components in step 1008. The first and second blade sides are substantially flat metal plates having lower current densities than the active edge. In this manner, the lower current densities of the first and second blade sides cause further modification (e.g., coagulation) of the previously modified (e.g., severed) target tissue (step 1012).

Fig. 43B schematically represents a number of steps involved in a method of severing tissue with an electrosurgical probe via a process involving molecular dissociation of tissue components, and of coagulating the severed tissue with the same electrosurgical probe during a single procedure, according to one embodiment of the invention. The electrosurgical probe typically comprises an active electrode in the form of a single, substantially flat metal hook or blade having at least one active edge adapted for electrosurgically severing the tissue, and first and second blade sides adapted for effecting hemostasis of the severed tissue. Steps 1000' through 1006' are substantially the same or analogous to steps 1000 through 1006, as described hereinabove with reference to Fig. 43A. Step 1008' involves severing the target tissue via localized molecular dissociation of tissue components due to high current densities generated at the position of an active edge upon execution of step 1004'. Step 1010' involves engaging the first and second blade

sides against the tissue severed in step 1008', whereby blood/blood vessels in the severed tissue are coagulated as a result of the relatively low current densities on the first and second blade sides (step 1012').

Fig. 44 schematically represents a number of steps involved in a method of dissecting a tissue or organ of a patient with an electrosurgical probe having a hook or blade active electrode, according to one embodiment of the invention, wherein step 1100 involves accessing an organ or tissue. Typically, accessing an organ or tissue in step 1100 involves incising an overlying tissue which conceals the organ or tissue to be dissected. As an example, in an open chest procedure involving a median sternotomy, the thoracic cavity is accessed by making a longitudinal incision through the sternum. Incising an overlying tissue in step 1100 may be performed generally according to the methods described with reference to Figs. 43A or 43B. Step 1102 involves positioning the distal end of the electrosurgical probe, and in particular an active edge of the hook or blade active electrode, in at least close proximity to connective tissue adjacent to the tissue or organ to be dissected. As an example, the connective tissue may be soft tissue, such as adipose tissue, or relatively hard tissue such as cartilage or bone. Optional step 1104 involves delivering an electrically conductive fluid to the distal end of the probe such that the electrically conductive fluid forms a current flow path between the active electrode and the return electrode, generally as described for step 1002, *supra*. Step 1106 involves applying a high frequency voltage between the active electrode and the return electrode, generally as described for step 1004, *supra*.

Depending on the type of procedure, e.g., the nature of the tissue or organ to be dissected, optional step 1108 may be performed, in which the probe is manipulated such that an active edge of the active electrode is moved with respect to the connective tissue adjacent to the tissue or organ to be dissected. Where the active electrode comprises a hook, the hook may be engaged against the connective tissue and drawn towards the operator of the probe to precisely control the degree of cutting or tissue removal. Step 1110 involves electrosurgically ablating, via molecular dissociation of connective tissue components, at least a portion of the connective tissue adjacent to the tissue or organ to be dissected. As an example, connective tissue adjacent to the internal mammary artery may be dissected by a

process involving molecular dissociation of connective tissue components, in either an open-chest or a minimally invasive procedure, such that the IMA is substantially free from connective tissue over a portion of its length.

Fig. 45A is a block diagram schematically representing an
 5 electrosurgical system 1200 including an electrosurgical probe 1201 and a high frequency power supply 1250. Probe 1201 includes an active electrode 1212 coupled to a first pole of high frequency power supply 1250. Probe 1201 further includes a first return electrode 1218 and a second return electrode 1270 coupled to a second pole of high frequency power supply 1250. Typically, high frequency
 10 power supply 1250 is adapted for operation in the ablation mode and the sub-ablation mode. Active electrode 1212 is adapted for ablating, cutting, severing, or dissecting tissue in the ablation mode, and for coagulating, contracting, welding, or otherwise modifying tissue in the sub-ablation mode. High frequency power supply 1250 may be readily switched between the ablation mode and the sub-ablation mode
 15 by the surgeon during operation of system 1200, for example, using one or more foot pedals (e.g., Fig. 1). Typically, first return electrode 1218 is fixed in relation to active electrode 1212. In contrast, second return electrode 1270 is typically movable with respect to active electrode 1212 (e.g., Figs. 47A-B, 59A-B).

Fig. 45B is a block diagram schematically representing an
 20 electrosurgical system 1200', according to another embodiment of the invention. System 1200' includes those elements of system 1200 described hereinabove with reference to Fig. 45A. System 1200' additionally includes a contact unit 1280 coupled between second return electrode 1270 and high frequency power supply 1250. Contact unit 1280 allows for the electrical coupling and uncoupling of second
 25 return electrode 1270 to high frequency power supply 1250. In one embodiment, electrical coupling and uncoupling of second return electrode 1270 via contact unit 1280 is determined by the location of second return electrode 1270 in relation to active electrode 1212 (e.g., Figs. 48A-B). In another embodiment, electrical coupling and uncoupling of second return electrode 1270 via contact unit 1280 may
 30 be controlled by an operator-actuated switch, e.g., a button, mounted on the probe.

Fig. 46 is a block diagram schematically representing an electrosurgical probe 1300, according to the invention. Probe 1300 includes a fixed

electrode assembly 1320 and a handle 1304 housing a connection block 1306.

Assembly 1320 includes an active electrode 1312 and a fixed return electrode 1318, both coupled to connection block 1306. Probe 1300 further includes a movable return electrode 1370 also coupled to connection block 1306. Connection block 1306 provides a convenient mechanism for coupling each of active electrode 1310, fixed return electrode 1318, and movable return electrode 1370 to a high frequency power supply (e.g., Figs. 1, 45A). Probe 1300 further includes an actuator unit 1390, in communication with movable return electrode 1370, for moving movable return electrode 1370. Typically, movable return electrode 1370 is movable linearly with respect to active electrode 1312 (e.g., Figs. 47A-49B).

Figs. 47A and 47B schematically represent an electrosurgical probe 1400, according to one embodiment of the invention. Probe 1400 includes a shaft 1402 having a shaft distal end 1402a, and a shaft proximal end 1402b. A handle 1404 is affixed to shaft proximal end 1402b. Handle 1404 houses a connection block 1406. A fixed return electrode 1418 is disposed at shaft distal end 1402a. An electrically insulating spacer 1410 extends distal to fixed return electrode 1418, and an active electrode terminal 1412 is disposed distal to spacer 1410. Active electrode terminal 1412 is coupled to connection block 1406 via an active electrode lead 1413. As shown, active electrode terminal 1412 is in the form of a hook. In one embodiment, the active electrode terminal comprises a flattened wire and a proximal end of the wire is coupled directly to the connection block. Other configurations for the active electrode terminal are also within the scope of the invention.

Again with reference to Figs. 47A-B, probe 1400 further includes a movable return electrode 1470. As shown, movable return electrode 1470 is coupled to connection block 1406 via a push rod 1471 and a second return lead 1476. In one embodiment, a proximal portion of push rod 1471 is ensheathed within an electrically insulating sleeve, and an exposed (non-insulated), distal portion of rod 1471 defines return electrode 1470. Movable return electrode 1470 is movable linearly with respect to active electrode terminal 1412 in a direction substantially parallel to the longitudinal axis of shaft 1402. Movable return electrode 1470 may be moved between (i) a distal location (Fig. 47A), in which movable return electrode 1470 is adjacent to active electrode terminal 1412, and (ii)

a proximal location (Fig. 47B), in which movable return electrode 1470 is retracted, e.g., within shaft 1402. In the distal location, movable return electrode 1470 defines a primary current path from active electrode terminal 1412 to the power supply (e.g., Figs. 1, 45A, 45B). In the retracted (proximal) location, movable return electrode 1470 is mechanically disengaged, or physically separated, from active electrode terminal 1412, and no longer provides a substantial current path from active electrode terminal 1412 to the power supply. The distal location of movable return electrode 1470 (Fig. 47A) represents a closed configuration of probe 1400, while the proximal location of movable return electrode 1470 (Fig. 47B) represents an open configuration of probe 1400. When probe 1400 is in the open configuration, fixed return electrode 1418 provides the primary current path from active electrode terminal 1412 to the power supply. The distal end of movable return electrode 1470 may be beveled at an angle, e.g., of about 45°, and active electrode terminal 1412 may be configured at a corresponding or complementary angle.

Once again with reference to Figs. 47A-B, moveable return electrode 1470 may be moved between the distal location and the proximal location via an actuator unit 1490. As shown, actuator unit 1490 is located on handle 1404. However, actuator unit 1490 may alternatively be located at other locations, e.g., on shaft proximal end 1402b. Moveable return electrode 1470 may be moved distally towards the closed configuration to capture, clamp, and weld or coagulate a blood vessel (e.g., Figs. 53A-C) during a broad range of surgical procedures. In the open configuration, active electrode terminal 1412 is adapted for cutting, dissecting, and severing a tissue or organ. In the closed configuration (distal location), a gap exists between the distal end of movable return electrode 1470 and a proximal face of active electrode terminal 1412. The gap in the closed configuration is typically in the range of from about 0.2 mm to 2 mm. In the open configuration (proximal location), movable return electrode 1470 is retracted and separated from active electrode terminal 1412 by a greater distance, typically in the range of from about 5 mm to 3 cm.

Figs. 48A and 48B schematically represent an electrosurgical probe 1500, according to another embodiment of the invention. Probe 1500 includes a

number of elements which are the same as, or analogous to, those described for probe 1400 with reference to Figs. 47A-B. Thus, probe 1500 includes a shaft 1502 having a shaft distal end 1502a, and a shaft proximal end 1502b; a handle 1504 affixed to shaft proximal end 1502b; a connection block 1506; a fixed return electrode 1518 disposed at shaft distal end 1402a; an electrically insulating spacer 1510 extending to a location distal to fixed return electrode 1518; and an active electrode terminal 1512 disposed distal to spacer 1510. Active electrode terminal 1512 and fixed return electrode 1518 are independently coupled to connection block 1506 via electrode leads (not shown). During use, probe 1500 is electrically coupled to a high frequency power supply (e.g., Fig. 1) via connection block 1506.

Again with reference to Figs. 48A-B, probe 1500 also includes a movable return electrode 1570. Typically, movable return electrode 1570 is movable linearly in a direction substantially parallel to the longitudinal axis of shaft 1502, between a distal location (Fig. 48A) and a proximal location (Fig. 48B). A proximal portion of movable return electrode 1570 comprises a movable rod or push rod 1571. As shown, rod 1571 lies external to shaft 1502. In one embodiment, rod 1571 comprises an electrically insulated portion 1574, and an electrically conducting zone 1572 proximal to insulated portion 1574. Probe 1500 further includes a contact unit 1580 coupled to connection block 1506 via a second return lead 1576. Contact unit 1580 may be in the form of a cylinder of electrically conducting material which makes electrical contact with movable return electrode 1570 when electrically conducting zone 1572 lies within contact unit 1580 (Fig. 48A). Thus, when probe 1500 is in the closed configuration, movable return electrode 1570 is electrically coupled to connection block 1506. Conversely, when electrically conducting zone 1572 is moved proximal of contact unit 1580 (Fig. 48B), movable return electrode 1570 is electrically uncoupled from connection block 1506. Moveable return electrode 1570 may be moved between the distal location and the proximal location via an actuator unit (not shown in Figs. 48A-B). In the distal location, movable return electrode 1570 defines a primary current path from active electrode terminal 1512 to the power supply. In the retracted position (proximal location or open configuration), movable return electrode 1570 is electrically disengaged from connection block 1506, and no longer provides a current path from

active electrode terminal 1512 to the power supply. In which case, fixed return electrode 1518 provides a current path from active electrode terminal 1512 to the power supply. In the open configuration, active electrode terminal 1512 is adapted for cutting, dissecting, and severing a tissue or organ. In the closed configuration, probe 1500 is adapted for the capture, clamping, and welding or coagulation of a blood vessel during various surgical procedures (e.g., Figs. 53A-C).

Figs. 49A and 49B schematically represent an electrosurgical probe having a return electrode movable between electrical engagement and electrical disengagement, according to another embodiment of the invention. Probe 1600 is somewhat analogous, both structurally and functionally, to probe 1500 described hereinabove with reference to Figs. 48A-B. Thus, probe 1600 includes a shaft 1602 having a shaft distal end 1602a, and a shaft proximal end 1602b; a handle 1604 affixed to shaft proximal end 1602b; a connection block 1606; a fixed return electrode 1618 disposed at shaft distal end 1602a; an electrically insulating spacer 1610 extending to a location distal to fixed return 1618; and an active electrode terminal 1612 extending distal to spacer 1610. Probe 1600 also includes a movable return electrode 1670 movable linearly in a direction substantially parallel to the longitudinal axis of shaft 1602 between an electrically coupled distal location (Fig. 49A), and an electrically uncoupled proximal location (Fig. 49B). Active electrode terminal 1612 and fixed return electrode 1618 are independently coupled to connection block 1606 via electrode leads (not shown). In use, probe 1600 is coupled to a high frequency power supply (e.g., Figs. 1, 45A-B) via connection block 1606. The mechanism shown for electrically coupling and uncoupling movable return electrode 1670 is analogous to that of the embodiment described with reference to Figs. 48A-B. Thus, a movable push rod 1671 comprises an electrically insulated portion 1674, and a proximal electrically conducting zone 1672. Contact unit 1680 is coupled to connection block 1606 via a second return lead 1676. Moveable return electrode 1618 is electrically coupled to connection block 1606 when electrically conducting zone 1672 lies within contact unit 1680 (Fig. 49A), i.e., when probe 1600 is in the closed configuration. On the other hand, in the open configuration movable return electrode 1670 is electrically uncoupled from connection block 1606. In contrast to the embodiment of Figs.

48A-B, in the embodiment of Figs. 49A-B, push rod 1671 lies internal to shaft 1602. Moveable return electrode 1670 may be moved between the distal location and the proximal location via an actuator unit (not shown in Figs. 49A-B). In one embodiment, the actuator unit may take the form of a slidable attachment (not shown) located on handle 1604.

Fig. 50 is a block diagram schematically representing an electrosurgical probe 1300', according to another embodiment of the invention. Probe 1300' includes a shaft 1302 and an electrically insulating tube 1303 lying within, and extending distally from, shaft 1302. A distal portion of electrically insulating tube 1303 protruding distally from shaft 1302 defines a first spacer 1308 (e.g., Fig. 51A, Fig. 52C). In one embodiment, electrically insulating tube 1303 comprises a multi-lumen plastic tube formed by an extrusion process (e.g., Figs. 56A-C, 58A-59B). Probe 1300' further includes a fixed return electrode 1318', and an active electrode terminal 1312' disposed on a second spacer 1310. In one embodiment, second spacer 1310 extends distally from an internal lumen of first spacer 1308. Probe 1300' still further includes a movable return electrode 1370', and an actuator unit 1390 for moving movable return electrode 1370' with respect to active electrode terminal 1312', between a distal location and a proximal location. Typically, movable return electrode 1370' is movable in a direction parallel to the longitudinal axis of shaft 1302, as described hereinabove (e.g., with reference to Figs. 47A-B). In one embodiment, probe 1300' is configured such that movable return electrode 1370' slides external to tube 1303 and within (internal to) shaft 1302 (e.g., Figs. 52A-C).

Fig. 51A schematically represents an electrosurgical probe 1700 having a linearly movable return electrode 1770, wherein movable return electrode 1770 is shown in a proximal location. The proximal location of movable return electrode 1770 defines an open configuration of probe 1700. Fig. 51B schematically represents the distal or working end of probe 1700 showing movable return electrode 1770 in a distal location (closed configuration). Probe 1700 includes a shaft 1702 having a shaft distal end 1702a and a shaft proximal end 1702b, and a handle 1704 affixed to shaft proximal end 1702b. An electrically insulating multi-lumen tube 1703 lies within, and extends distally from, shaft 1702.

A distal portion of tube 1703 protruding from shaft distal end 1702a defines a first electrically insulating spacer 1708. A fixed return electrode 1718 is disposed on first spacer 1708. Tube 1703 serves as a spacer to separate, or space, fixed return electrode 1718 from movable return electrode 1770. First electrically insulating spacer 1708 may extend from shaft distal end 1702a by a distance in the range of from about 0.3 to 2.5 inches, and more typically from about 0.5 to 2.0 inches. As shown, fixed return electrode 1718 is in the form of a coil. As an example, return electrode 1718 may be a coil of wire having from about three (3) to ten (10) turns (e.g., Figs. 57A-C). A second electrically insulating spacer 1710 lies within the coil of return electrode 1718. An active electrode terminal 1712 extends distally from second spacer 1710 at an angle of about 45°. Other shapes and configurations for the fixed return electrode and the active electrode are also within the scope of the invention.

Again with reference to Figs. 51A, 51B, movable return electrode 1770 may be mechanically disengaged, i.e., rendered non-functional as a return electrode, by being retracted within shaft 1702. Additionally, or alternatively, movable return electrode 1770 may alternate between electrical coupling and electrical uncoupling by translation of movable return electrode 1770 between the distal location of Fig. 51B, and the proximal location of Fig. 51A, respectively. As an example, movable return electrode 1770 may be electrically coupled and uncoupled to a connection block via a mechanism analogous to that described with reference to Figs. 49A-B. Fig. 51C is a sectional view taken along the lines 51C-51C of Fig. 51A, showing movable return electrode 1770 disposed internal to shaft 1702 and external to multi-lumen tube 1703. Internal lumina of tube 1703 are omitted from Fig. 51C for the sake of clarity. As shown in Fig. 51C, movable return electrode 1770 is semicircular in cross-section, however other configurations for the movable return electrode are also within the scope of the invention (e.g., Figs. 54A-C).

Figs. 52A-C show the distal or working end of an electrosurgical probe 1800, as seen from an inferior location. Fig. 52A shows probe 1800 in a closed configuration, with a movable return electrode 1870 extending distally from shaft 1802 to a distal location such that movable return electrode 1870 lies adjacent

to an active electrode terminal 1812. In the closed configuration, movable return electrode 1870 defines the primary current path from active electrode terminal 1812. (Active electrode terminal 1812 is partially obscured by return electrode 1870 in Fig. 52A.) Moveable return electrode 1870 may have a circular or semi-circular cross-sectional shape and a beveled or straight distal end. Moveable return electrode 1870 may comprise a metal such as stainless steel, platinum, molybdenum, tungsten, palladium, iridium, titanium, or their alloys.

Fig. 52B shows probe 1800 having movable return electrode 1870 partially retracted to reveal a portion of a first electrically insulating spacer 1808, a fixed return electrode 1818 disposed distal to first spacer 1808, and a second electrically insulating spacer 1810 extending distal to fixed return electrode 1818. First spacer 1808 serves to separate, isolate, or space fixed return electrode 1818 from movable return electrode 1870. Fig. 52C shows probe 1800 in an open configuration, with movable return electrode 1870 retracted within shaft 1802. In the open configuration, fixed return electrode 1818 defines the primary current path from active electrode terminal 1812. Thus, the current path from active electrode terminal 1812 can be manipulated, adjusted, or determined by changing the location of movable return electrode 1870 with respect to active electrode terminal 1812. The location of movable return electrode 1870 may be changed via an actuator unit (e.g., Fig. 46). As an example, an actuator unit may comprise a thumb-piece (not shown) affixed to movable return electrode 1870 and mounted on probe 1800, wherein movable return electrode 1870 may be moved back and forth between a distal location and a proximal location by pulling and pushing on the thumb-piece. Other mechanisms for moving or sliding a rod or cylinder within a hollow shaft are well known in the art. In one embodiment, shaft 1802 comprises a metal tube, e.g., comprising stainless steel, having an electrically insulating coating over the entire external surface of the metal tube. In an alternative embodiment, shaft 1802 comprises a rigid or flexible electrically insulating material, for example, a tube comprising various plastics, such as a polycarbonate, a polyimide, a fluoropolymer, or a polyurethane.

Figs. 53A-C schematically represent an active electrode terminal 1912 and a linearly movable return electrode 1970 of an electrosurgical probe of the

invention, in relation to a blood vessel, BV. As an example, blood vessel, BV may be a vessel encountered by a surgeon during cutting or resection of tissue, wherein cessation of blood flow within the vessel may be required prior to severing the vessel. Linear movement of movable return electrode 1970 toward active electrode terminal 1912 is indicated by the solid arrow. Moveable return electrode 1970 may be moved in the indicated direction by actuation of an actuator unit (e.g., Figs. 46, 47A-B). Fig. 53B shows the probe in the closed configuration, with blood vessel, BV' compressed between active electrode terminal 1912 and movable return electrode 1970. In the closed configuration, movable return electrode 1970 may be continuously urged in the distal direction, e.g., by actuation of the actuator unit, to effectively clamp and compress the blood vessel. Compression of blood vessel, BV' (Fig. 53B) prevents blood flow through vessel, BV', and shortens the distance (i.e., the current path) between active electrode terminal 1912 and movable return electrode 1970. The shorter current path leads to a higher current density between active electrode terminal 1912 and movable return electrode 1970. At the same time, stopping blood flow within blood vessel, BV' prevents cooling normally associated with flow of blood within the vessel.

After blood vessel, BV' has been clamped and compressed (Fig. 53B), a high frequency voltage may be applied between active electrode terminal 1912 and movable return electrode 1970 to weld or coagulate the blood vessel. Typically, the high frequency voltage is applied from a high frequency power supply in the sub-ablation mode to provide controlled localized heating of blood vessel, BV'. In this way, the walls of the blood vessel may be welded together, e.g., by cross-linking of collagen fibers. As a result, the coagulated blood vessel, BV'' remains occluded after movable return electrode 1970 is retracted to the open configuration (Fig. 53C). Subsequently, occluded blood vessel, BV'' may be severed, e.g., via active electrode terminal 1912, while maintaining hemostasis at the surgical site.

Fig. 54A shows a longitudinal section of a movable return electrode/push rod assembly 2072 for an electrosurgical probe of the invention. Assembly 2072 includes a distal end 2072a and a proximal end 2072b. Assembly 2072 comprises a body 2076, and an electrically insulating sleeve 2074, which

ensheathes a proximal portion of body 2076. An exposed (non-insulated) distal portion of assembly 2072 defines a movable return electrode 2070. The exposed distal portion of assembly 2072 defining movable return electrode 2070 typically has a length in the range of from about 0 (zero) mm to 10 mm, more typically from about 0 to 5 mm, and often from about 2 mm to 4 mm. Distal end 2072a is beveled at an angle of about 45° as shown. Other angles for distal end 2072a are also possible under the invention. Proximal end 2072b may be coupled directly to a connection block of the probe, or may be coupled to the connection block via a return electrode lead (e.g., Figs. 47A-B). Fig. 54B is a transverse sectional, taken at the lines 54B-54B of Fig. 54A, showing the circular cross-sectional shape of assembly 2072, according to one embodiment. Typically, movable return electrode 2070 has the same, or a similar, cross-sectional shape as assembly 2072. Body 2076 is shown as a cylinder in Figs. 54A-B, however, in some embodiments body 2076 could be a solid rod. Furthermore, in other embodiments the distal end of the body may be straight (non-beveled).

Fig. 54C is a side view of movable return electrode 2070, in relation to an active electrode terminal 2012 of an electrosurgical probe in the closed configuration. Active electrode terminal 2012 includes an arm 2013 and a crosspiece 2014. The distal end of return electrode 2070 lies adjacent to a proximal face of crosspiece 2014. Electrically insulating sleeve 2074 is omitted from Fig. 54C for the sake of clarity.

Fig. 54D shows a longitudinal section of a movable return electrode/push rod assembly 2072' for an electrosurgical probe of the invention. Assembly 2072' is somewhat analogous to assembly 2072 of Fig. 54A. Thus, assembly 2072' includes a distal end 2072'a and a proximal end 2072'b, a body 2076', and an electrically insulating sleeve 2074'. In the embodiment of Fig. 54D, the entire length of body 2076' is ensheathed by sleeve 2074'. An exposed (non-insulated) distal edge of body 2076' defines a movable return electrode 2070'. In alternative embodiments, distal end 2072'a may be beveled at various angles. Fig. 54E is a cross-sectional view, taken at the lines 54E-54E of Fig. 54D, showing the circular cross-sectional shape of movable return electrode 2072'. Body 2076' is shown as a rod in Figs. 54D-E, however, in some embodiments the body could be a

metal cylinder, e.g., a stainless steel tube. Furthermore, in other embodiments the distal end of the body may be exposed (non-insulated) to define a movable return electrode having a larger surface area.

Fig. 54F shows a longitudinal section of a movable return electrode/push rod assembly 2072'' for an electrosurgical probe, somewhat analogous to assembly 2072 of Figs. 54A-B. Thus, assembly 2072'' includes a distal end 2072''a and a proximal end 2072''b, a body 2076'', and an electrically insulating sleeve 2074''. An exposed (non-insulated) distal end of body 2076'' defines a movable return electrode 2070''. In alternative embodiments, distal end 2072''a may be straight or non-beveled. As shown in Fig. 54E assembly 2072'' has a semi-circular cross-sectional shape. Typically, movable return electrode 2070'' has the same, or a similar, cross-sectional shape as assembly 2072''. In one embodiment, movable return electrodes/push rod assemblies of the invention, e.g., assembly 2072'', may be formed from a metal cylinder by removing portions of the cylinder to provide a desired configuration.

Figs. 55A-B schematically represent a hook-like active electrode terminal 2112 for an electrosurgical probe of the invention. Active electrode terminal 2112 includes an arm 2113, and a crosspiece 2114 arranged at an angle θ with respect to arm 2113. In the embodiment shown in Figs. 55A-B, angle θ is typically in the range of from about 85° to 95°, and often about 90°. Typically, arm 2113 lies substantially parallel to the longitudinal axis of the probe shaft. Crosspiece 2114 includes a proximal face 2114a, a distal face 2114b, and an apex or apical portion 2114c. Each of proximal face 2114a, distal face 2114b, and apex 2114c may be used for electrosurgically severing a tissue or organ of a patient. In addition, proximal face 2114a is adapted for opposing a distal end of a movable return electrode, for the purpose of clamping a target tissue, blood vessel, etc. (e.g., Fig. 53B). Fig. 55B shows distal face 2114b as seen along the lines 55B-55B of Fig. 55A, and indicating first and second sides, 2114d, 2114e, respectively.

Fig. 55C schematically represents a hook-like active electrode terminal 2112', according to another embodiment of the invention. Active electrode terminal 2112' includes an arm 2113' and a crosspiece 2114', somewhat analogous

to active electrode terminal 2112 (Fig. 55A). In the embodiment of Fig. 55C crosspiece 2114' is arranged at an angle Π' with respect to arm 2113, wherein angle Π' is typically in the range of from about 40° to 50°, usually from about 35° to 55°, and often about 45°. Crosspiece 2114' includes a proximal face 2114'a, a distal face 2114'b, and an apex 2114'c somewhat analogous to those of electrode terminal 2212 (Fig. 55A).

Figs. 55D, 55E, and 55F show a perspective view, a side view, and an end view, respectively, of a hook-like active electrode 2212, according to another embodiment of the invention. An active electrode filament 2213 comprises a pair of juxtaposed wires 2213a, 2213b. An active electrode terminal 2214 comprises a first branch 2216a and a second branch 2216b defining a void 2217 therebetween. First branch 2216a and second branch 2216b meet at an apex or apical portion 2216c. First branch 2216a and second branch 2216b are separated by a first distance, D_1 adjacent to filament 2213, tapering to a second distance D_2 adjacent to apex 2216c. Typically, distance D_1 is in the range of from about 0.010 inch to 0.050 inch, often from about 0.020 inch to 0.035 inch. Typically, distance D_2 is in the range of from about 0.005 inch to 0.020 inch, often from about 0.005 inch to 0.015 inch. Void 2217 is adapted for retaining a fluid between first and second branches 2216a,b. Void 2217 is further adapted for transporting a liquid within void 2217, either towards or away from apex 2216c, e.g., via capillary action. As shown, terminal 2214 comprises a shaped wire having a substantially planar distal face 2214b and a substantially planar proximal face 2214a. Planar surfaces on terminal 2214 facilitate grasping of tissue between terminal 2214 and a movable return electrode (e.g., Figs. 53A-C). Typically, terminal 2214 has at least two contiguous planar surfaces to provide an angular geometry, which promotes high current densities at terminal 2214.

Fig. 56A schematically represents a multi-lumen tube 2403 as seen in perspective view, according to one aspect of the invention. Multi-lumen tube 2403 includes a distal face 2408 and a plurality of internal lumina represented as lumina 2442a, 2442b, 2442n. Each lumen terminates at distal face 2408 in a corresponding port 2462a, 2462b, 2462n. Multi-lumen tube 2403 may comprise an electrically insulating plastic tube, which may be formed, for example, by injection molding,

blow molding, or by an extrusion process. Internal lumina, e.g., 2442a-n, may accommodate a proximal portion of a return - or active electrode, or may house an electrode lead of a return - or active electrode (e.g., Fig. 57B). In addition, one or more of the internal lumina may serve as a conduit for an electrically conductive fluid, and/or for aspiration of excess materials from the surgical site via an aspiration stream (e.g., Figs. 58A-B). The number of lumina within multi-lumen tube 2403 is typically from two to four.

Fig. 56B is a perspective view of a multi-lumen tube 2403' of an electrosurgical probe, according to one embodiment of the invention. Multi-lumen tube 2403' includes an end-plate or distal face 2408' and four internal lumina represented as lumina 2442'a-d. Each lumen terminates at distal face 2408' in a corresponding port 2462'a-d. Multi-lumen tube 2403' typically comprises an electrically insulating plastic tube, formed, for example, by an extrusion process. Internal lumina 2442'a and 2442'b may accommodate an active electrode and a return electrode, respectively. Internal lumina 2442'c and 2442'd may serve as a fluid delivery lumen and as an aspiration lumen, respectively. Fluid delivery lumen 2442'c serves as a conduit for discharging an electrically conductive fluid from fluid delivery port 2462'c. Aspiration lumen 2442'd serves to remove excess or unwanted materials from the surgical site via aspiration port 2462'd.

Fig. 56 C is an end view of multi-lumen tube 2403' of Fig. 56B showing the location of ports 2442'a-d of tube 2403' in relation to a shaft 2402' of a probe. Fig. 57D is an end view showing the location of an active electrode filament 2413 and a return electrode 2418' in relation to ports 2442'a-d of multi-lumen tube 2403'. Return electrode 2418' is schematically represented in Fig. 56D as circular dashed lines. The dashed circle representing return electrode 2418' encompasses a portion of fluid delivery port 2462'c. Active electrode filament 2413 lies within the dashed circle representing return electrode 2418'. The configuration shown in Fig. 56D promotes contact of an electrically conductive fluid delivered from port 2462'c with the electrode assembly (active and return electrodes). Active electrode filament 2413 is depicted in Fig. 56D as a pair of juxtaposed round wires (e.g., Figs. 55D, 55F). However, other configurations for an active electrode filament, e.g., a single wire, are also within the scope of the invention.

Fig. 57A is a side view of a return electrode, shown in relation to distal end 2503a of a multi-lumen tube 2503 of an electrosurgical probe, according to one embodiment of the invention. The return electrode comprises a return electrode filament 2524, and a distal return electrode terminal or head 2522. Return electrode head 2522 is in the form of a coil. As shown, return electrode head 2522 comprises about 6 turns, however, other number of turns may also be used. Typically, return electrode head 2522 will comprise up to about 100 turns, and more typically from about 3 to 10 turns. Return electrode filament 2524 and return electrode head 2522 may be formed from a length of wire comprising a metal such as molybdenum, platinum, tungsten, palladium, iridium, titanium, or their alloys. As shown, the coil (or return electrode head 2522), and the axial space defined by the coil, are substantially cylindrical. Alternatively, the coil of return electrode head 2522, and hence the axial space, may have other shapes, e.g., frusto-conical shapes defined by tapering or expansion of the coil. For example, the coil may either taper or expand as it is wound in the proximal direction.

Again with reference to Fig. 57A, the coil of return electrode head 2522 has a pitch, P, which is usually in the range of from about 0.010 to 0.150 inch, more typically from about 0.010 to 0.045 inch, and more often from about 0.012 to 0.025 inch. Generally, the maximum pitch corresponds to about five times the diameter of the wire used to wrap the coil, while the minimum pitch equals the diameter of the wire used to wrap the coil (as described hereinbelow). As shown, a gap 2523 exists between each turn of return electrode head 2522. The turns of the coil form an open wall having a spiral opening comprising the plurality of gaps 2523. Gaps 2523 allow an electrically conductive liquid, e.g., isotonic saline, to flow between the turns of return electrode head 2522, whereby both interior and exterior portions of return electrode head 2522 may be wetted by the electrically conductive liquid. Gap 2523 also promotes retention of electrically conductive liquid, e.g., via surface tension. In an alternative embodiment (not shown), the coil of the return electrode head is wound such that no gap exists between the turns of the coil, i.e., the wire of each succeeding turn is in contact with the preceding turn, resulting in a return electrode terminal or head having a cylindrical or quasi-cylindrical wall. In the latter embodiment, the pitch of the coil

can be considered to be the diameter of the wire used to wind the coil. Typically, return electrode head 2522 has an external diameter, D in the range of from about 0.050 to 0.200 inch, and more usually from about 0.070 to 0.150 inch. Return electrode filament 2524 is accommodated within a return electrode lumen 2542a within tube 2503. Typically, return electrode filament 2524 is ensheathed within an electrically insulating coating (not shown), e.g., a layer of a polyimide. Only lumen 2542a is shown in Fig. 57A, for the sake of clarity.

Fig. 57B is a side view of a distal portion of an electrosurgical probe 2500, incorporating the return electrode of Fig. 57A. Probe 2500 includes an active electrode filament 2534 and an active electrode head or terminal 2532. Active electrode filament 2534 is accommodated within an active electrode lumen 2542b of tube 2503. A distal portion of active electrode filament 2534 is encircled within an electrically insulating spacer 2516. (Spacer 2516 can be considered as analogous to the second spacer of the embodiments of Figs. 50-52C, while a distal portion of tube 2503 can be considered as analogous to the first spacer of the embodiments of Figs. 50-52C.) As shown, the proximal portion of spacer 2516 is inserted within the distal end of lumen 2542b. Spacer 2516 and the distal portion of active electrode filament 2534 lie within return electrode head 2522. Typically, return electrode head 2522 is fixed in relation to active electrode terminal 2532. Active electrode terminal 2532 may be in the form of a hook, or a shaped, flattened, and/or bent wire (e.g., Figs. 55A-F). The surface area of the return electrode coil is usually at least about twice (i.e. 2X) the surface area of the active electrode terminal; and more typically, from about two times to about 20 times (20X) the surface area of the active electrode terminal. The relatively large surface area of the return electrode coil prevents inadvertent firing of the return electrode during use of the probe.

Fig. 57C is an end view of return electrode head 2522 of Fig. 57B, indicating the positions of return electrode filament 2524 and free end 2526 within return electrode head 2522, i.e., at approximately six o'clock and nine o'clock, respectively. Thus, free end 2526 lies within an axial space 2528 of return electrode head 2522. However, other arrangements for return electrode filament 2524 and free end 2526 in relation to return electrode head 2522 are also possible

under the invention. Spacer 2516 also lies within axial space 2528, and may comprise a cylinder of a glass, or a ceramic, e.g., alumina. Active electrode filament 2534 lies within spacer 2516. As shown, a substantially cylindrical void 2518 exists between active electrode filament 2534 and the inner wall of spacer 2516. Active electrode terminal 2532 is omitted from Fig. 57C for the sake of clarity.

Fig. 58A is a face view, and Fig. 58B is a longitudinal section, of the distal end 2603a of a multi-lumen tube 2603, according to one embodiment of the invention. A fluid delivery port 2662c is situated on a distal face 2608 of tube 2603. As shown in Fig. 58B, fluid delivery port 2662c is in communication with a fluid delivery lumen 2642c. Typically, fluid delivery lumen 2642c is coupled to a proximal fluid delivery tube (e.g., Fig. 40A). Fluid delivery port 2662c is adapted for delivering an electrically conductive fluid to a fixed electrode assembly 2620. Electrode assembly 2620 is disposed at tube distal end 2602b, and is represented generically in Figs. 58A-B as a rectangular shape. At least a portion of electrode assembly 2620 is aligned with fluid delivery port 2662c, such that an electrically conductive fluid (represented in Fig. 58B by solid arrows) emanating from fluid delivery port 2662c contacts electrode assembly 2620.

Again with reference to Figs. 58A-B, multi-lumen tube 2603 may also include an aspiration port 2662d and an aspiration lumen 2642d adapted for aspirating excess electrically conductive fluid and any unwanted materials, from the vicinity of the probe working end, via an aspiration stream (open arrows) flowing proximally within aspiration lumen 2642d. Typically, aspiration lumen 2642d is coupled to an aspiration tube (e.g., Fig. 40A), which in turn may be coupled to a suitable vacuum source. In one embodiment, aspiration lumen 2642d is coupled to a vacuum line or tube via a y-hub (not shown) connected to the proximal end portion of the probe shaft. Such a y-hub may comprise a plastic material, such as a polycarbonate, and the like. The flow rate of the aspiration stream within aspiration lumen 2642d may be controlled or adjusted via a valve or similar mechanism. Although tube 2603 is portrayed as circular in cross-section, other shapes for the multi-lumen tube are also within the scope of the invention (e.g., Figs. 56B-C).

Fig. 59A is a side view showing the working end of an electrosurgical probe 2700 in the open configuration. Probe 2700 includes a shaft 2702 having a shaft distal end 2702a. A multi-lumen tube 2703 extends distally from shaft 2702, and a fixed return electrode 2718 extends distally from multi-lumen tube 2703. Fixed return electrode 2718 is shown as a coil of wire, although other configurations are possible under the invention. Probe 2700 further includes a push rod 2771. In Fig. 59A push rod 2771 is shown as retracted within shaft 2702. An active electrode 2712 is disposed distal to fixed return electrode 2718. Push rod 2771 is movable linearly with respect to active electrode 2712. Push rod 2771 may comprise a metal rod or a metal cylinder, such as a stainless steel tube. A movable return electrode 2770 is disposed at the distal end of push rod 2771. In one embodiment, a proximal portion of push rod 2771 is ensheathed within an electrically insulating layer (e.g., Figs. 54A-G), and movable return electrode 2770 comprises an exposed distal portion of rod 2771.

Fig. 59B shows probe 2700 in the closed configuration, with rod 2771 advanced distally such that movable return electrode 2770 occupies a distal location adjacent to active electrode 2712. In the closed configuration probe 2700 is adapted for grasping tissue, clamping blood vessels, and for coagulating tissue and welding together the walls of blood vessels (e.g., Figs. 53A-C). Fig. 59C is a cross-sectional view of probe 2700 taken along the lines 59C-59C of Fig. 59B, and indicating the position of multi-lumen tube 2703 and push rod 2771 in relation to shaft 2702.

Fig. 60A schematically represents a number of steps involved in a method of electrosurgically treating (for example, ablating, cutting, contracting, coagulating, or otherwise modifying) a target tissue of a patient, wherein step 2800 involves providing an electrosurgical probe having a shaft, an active electrode, a fixed return electrode, and a movable return electrode. The movable return electrode is movable linearly with respect to the active electrode between a proximal location (open configuration of the probe) and a distal location (closed configuration of the probe) (e.g., Figs. 47A,B, 59A-B). In one embodiment, the movable return electrode is disposed at the distal end of a push rod movable in relation to the active electrode and the shaft, wherein the movable return electrode is completely

retractable within the shaft in the open configuration, and wherein the movable return electrode lies adjacent to the active electrode in the closed configuration. The probe provided in step 2800 may have other elements, features, or characteristics of the various embodiments described hereinabove (e.g., as described with reference to Figs. 45A-59C). In one embodiment, the active electrode comprises an electrode arm and a crosspiece in the form of a hook. Typically, the crosspiece is arranged at an angle in the range of from about 45° to 90° to the longitudinal axis of the shaft. In one embodiment, the active electrode comprises a pair of shaped wires forming a window or void between a first branch and a second branch of the electrode.

According to one aspect of the invention, the movable return electrode moves linearly in a direction substantially parallel to the longitudinal axis of the shaft in response to actuation of an actuator unit. In another aspect, the probe includes an electrically insulating multi-lumen tube lying within the shaft and protruding from the shaft distal end. The distal end of the multi-lumen tube defines a first electrically insulating spacer. The fixed return electrode is disposed distal to the multi-lumen tube, and the probe further includes a second electrically insulating spacer located distal to the fixed return electrode. In one embodiment, the fixed return electrode comprises a coil of wire having from about three to 10 turns.

Typically, the probe further includes a connection block adapted for coupling each of: the active electrode, the fixed return electrode, and the movable return electrode to a high frequency power supply (e.g., Fig. 1, Figs. 45A-B). The high frequency power supply is typically adapted for operation in the ablation mode and the sub-ablation mode, wherein the surgeon may conveniently switch between the ablation mode and the sub-ablation mode, e.g., using a foot pedal (as described hereinabove). In one embodiment, the probe provided in step 2800 features a multi-lumen plastic tube formed by an extrusion process. The multi-lumen tube may have a lumen for each of: fluid delivery to the distal or working end of the probe, aspiration of excess or unwanted materials from the surgical site, housing an active electrode filament or lead, and housing a filament or lead of the fixed return electrode.

Step 2802 involves positioning the active electrode of the probe in at least close proximity to the target tissue. In one embodiment, the active electrode

includes an active electrode terminal comprising a hook having a crosspiece adapted for cutting and coagulating tissue. The crosspiece is further adapted for cooperating with the movable return electrode to clamp a target tissue, organ, or blood vessel between a proximal face of the crosspiece and a distal end of the movable return electrode. In one embodiment, the active electrode has an elongated window or void adapted for retaining and transporting a liquid, e.g., isotonic saline, within the void. Optional step 2804 involves delivering an electrically conductive fluid, e.g., via a fluid delivery lumen and fluid delivery port, to the working (distal) end of the probe. In one embodiment, the fluid delivery port is aligned with at least a portion of the fixed return electrode, such that fluid is directed against at least one of the fixed return electrode and the active electrode. The electrically conductive fluid (e.g., isotonic saline) provides a current flow path between the active electrode and at least one of the fixed return electrode and the movable return electrode. In the open configuration, the primary current path is between the active electrode and the fixed return electrode. In the closed configuration, the primary current path is between the active electrode and the movable return electrode. In one embodiment, the probe is adapted for positioning the movable return electrode at various positions between the proximal location (open configuration) and the distal location (closed configuration). In this way the current path from the active electrode to the power supply can be adjusted or manipulated by the surgeon during a procedure.

Step 2806 involves applying, via the high frequency power supply, a high frequency voltage between the active electrode and at least one of the fixed return electrode and the movable return electrode, wherein the high frequency voltage is sufficient to treat, modify, coagulate, cut, or ablate the target tissue or organ. The high frequency power supply may be operated in the ablation mode or the sub-ablation mode, as described hereinabove, according to the desired effect on the target tissue, e.g., in the ablation mode for cutting and volumetric removal of tissue, and in the sub-ablation mode for coagulating or welding the tissue. The actual voltage applied in step 2806 will generally be within the ranges cited hereinabove, for example, from about 70 volts RMS to 500 volts RMS in the ablation mode, and from about 10 volts RMS to 90 volts RMS in the sub-ablation mode.

Step 2808 involves manipulating the probe with respect to the target tissue or organ. Typically, the probe includes a proximal handle, and the probe is manipulated in step 2808 via the handle. In one aspect, step 2808 may involve translating the probe in a direction substantially parallel to the longitudinal axis of the probe, whereby the target tissue is severed, excised, transected, resected, or cut. Alternatively or additionally, step 2808 may involve translating the probe in a direction substantially orthogonal to the longitudinal axis of the probe, whereby the target tissue is volumetrically removed or ablated. Typically, volumetric removal of target tissue according to the invention comprises plasma-induced molecular dissociation of target tissue components. Coagulation or hemostasis may be attained by applying a suitable sub-ablation voltage to the probe (during step 2806, *supra*) while engaging a blood vessel or target tissue against the active electrode terminal. By sub-ablation voltage is meant a voltage sufficient to coagulate, weld, or contract a tissue or blood vessel, but insufficient to vaporize and remove tissue. Step 2810 involves aspirating any unwanted materials (such as gaseous ablation by-products, excess electrically conductive fluid, and the like) from the surgical site.

Fig. 60B schematically represents a number of steps involved in a method of severing a tissue or organ of a patient, using an electrosurgical system including a probe and a high frequency power supply, wherein step 2900 involves clamping a target tissue by the probe. The probe provided in step 2900 may include various elements, features, or characteristics of the electrosurgical probes described hereinabove (e.g., as described with reference to Figs. 45A-59C). Typically, the probe includes a hook-like active electrode terminal, a fixed return electrode, and a movable return electrode linearly movable with respect to the active electrode terminal between a proximal location (open configuration) and a distal location (closed configuration). In one aspect of the invention, the target tissue may comprise a portion of a blood vessel. For example, during resection of connective tissue, the surgeon may encounter one or more relatively large blood vessels which require coagulation before proceeding with the resection. Upon encountering such a blood vessel, the surgeon may coagulate the blood vessel, as follows. With the electric power from the power supply turned off, or with the electrosurgical system operating in the sub-ablation mode, the blood vessel may be clamped between the

active electrode terminal and the movable return electrode in order to compress the vessel and to prevent blood flow at the region of compression, essentially as described hereinabove, e.g., with reference to Figs. 53A-C. Thereafter, with the electrosurgical system operating in the sub-ablation mode, step 2902 involves

5 applying a first high frequency voltage between the active electrode and the movable return electrode, wherein the first high frequency voltage is effective in welding or coagulating the blood vessel, but insufficient to ablate the blood vessel.

While the blood vessel or other target tissue remains clamped by the probe, step 2904 involves coagulating or welding the clamped blood vessel, or other

10 target tissue, as a result of the first high frequency voltage applied in step 2902. After coagulation has occurred to a suitable extent, optional step 2906 involves releasing or unclamping the clamped vessel or other target tissue from the probe. Typically, releasing the target tissue involves configuring the probe to the open, or partially open, configuration, e.g., by moving the movable return electrode in the

15 proximal direction via actuation of an actuator unit (e.g., Fig. 46). Thereafter, the electrosurgical system is switched to the ablation mode, and a second, ablation voltage is applied to the active electrode in step 2908, wherein the ablation voltage is sufficient to ablate the coagulated tissue.

With the probe in the open configuration, the probe may be

20 manipulated by the surgeon such that the active electrode is engaged against, and moved with respect to, the coagulated blood vessel or tissue, step 2910. Step 2912 involves severing the coagulated blood vessel or tissue via localized ablation of blood vessel/tissue components. In the example cited above, namely wherein a blood vessel is encountered during resection of a tissue, after the blood vessel has

25 been coagulated and severed according to steps 2900 through 2912, with the system operating in the ablation mode, the surgeon may then resume resection of tissue while maintaining hemostasis at the surgical site.

Fig. 60C schematically represents a number of steps involved in a method of severing a tissue using an electrosurgical instrument or probe, according

30 to another embodiment of the invention. Step 3000 involves applying an ablation level high frequency voltage between an active electrode terminal and a first return electrode of the probe, wherein the active electrode terminal is positioned in at least

close proximity to the tissue, and the ablation voltage is sufficient to sever the tissue due to the localized ablation of tissue in the vicinity of the active electrode terminal. During step 3000, the surgeon may encounter a blood vessel that requires severing, wherein blood flow within the vessel must be stopped prior to severing the vessel.

5 In which case, step 3002 involves engaging the blood vessel between the active electrode terminal and a second return electrode, such that the blood vessel is compressed. The second return electrode is movable linearly between a proximal location (representing an open configuration of the probe), and a distal location (representing a closed configuration of the probe). Typically, during step 3002 the
10 probe is in the closed configuration, or is being urged towards the closed configuration. Step 3004 involves applying a sub-ablation voltage between the active electrode terminal and the movable return electrode, wherein the voltage is sufficient to coagulate or weld the walls of the vessel, whereby the blood vessel is occluded and blood flow is prevented.

15 Step 3006 involves disengaging the second return electrode from the vessel. That is to say, the movable return electrode is moved in a proximal direction to configure the probe in the open, or partially open, configuration. In one embodiment, step 3006 involves moving the movable return electrode proximally, e.g., within an electrically insulated shaft of the probe, such that the movable return
20 electrode is physically separated from the working end of the probe, and the movable return electrode no longer provides a substantial current path from the active electrode terminal. In another embodiment, step 3006 involves moving the movable return electrode proximally, for example, in relation to a contact unit of the probe (e.g., Figs. 49A-B), such that the movable return electrode is electrically
25 uncoupled. When the movable return electrode is mechanically disengaged or electrically uncoupled from the probe, the first return electrode provides a current path from the active electrode terminal to the power supply. Step 3008 involves applying an ablation voltage to the active electrode terminal, wherein the coagulated blood vessel is severed at the location where the vessel was occluded as a result of
30 step 3004.

It is to be understood that the electrosurgical apparatus of the invention is by no means limited to those methods described in detail, e.g., with

